

Astronomers!

Do you know where your galaxies are?

Introducing the *Duchamp* Source Finder



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The Problem: Making the most of your surveys

Large-scale spectral-line radio surveys are an effective way to study populations of galaxies, masers, or sites of star-formation. Surveying on a large scale allows one to both probe to the fainter flux levels and remain sensitive to the rare but interesting objects at the brightest fluxes.

Effective use of large-scale surveys is dictated by the efficiency of detection of the objects of interest. Finding the extreme bright objects is often the easy bit – to find the more typical sources you need to push down to fainter fluxes close to the noise level. The complexity and volume of three-dimensional survey data also requires a large degree of automation and reliability to find the desired sources quickly and in a uniform way.

The Solution: The *Duchamp* Source Finder

Duchamp is our solution to the problem of three-dimensional source finding. It is a stand-alone software package, designed to work with spectral-line FITS cubes and produce source lists and graphical results showing detected objects.

Duchamp is optimised for the case of a large number of separated sources embedded in a cube dominated by noise – the typical situation expected for HI or maser surveys.

Innovations in Searching

A key aspect of source detection is the application of a threshold. This is calculated by using either a simple n -sigma cutoff, or derived through the use of the False Discovery Rate method¹, which controls the number of false detections. The statistics for the threshold calculations are obtained through robust methods, and can be measured from the full cube or a specified subset.

Searching in 3D is in general a complex problem. *Duchamp* approaches this by searching in each 2D channel map separately², and comparing detections made in one channel with those in neighbouring channels. An efficient merging algorithm then merges the 2D detections to form 3D objects.

Beating the noise

The limiting factor in detecting faint objects is the background noise, and *Duchamp* provides ways to minimise its effects. Simple smoothing before searching is possible, either spectrally using a Hanning filter, or spatially using a 2D Gaussian kernel.

Alternatively, the cube can be reconstructed using the à trous wavelet technique³. This filters the cube at a range of scales, thresholding each scale and only keeping those pixels with significant signal. This very effectively removes noise from the cube, allowing searching to be done on much cleaner data.

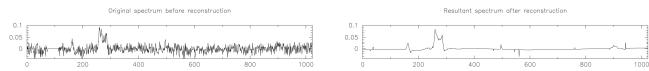


Figure 1: An example of the à trous algorithm used in one dimension to reconstruct a spectrum. Note the double-horned shape of the resultant main object, and the preservation of the weak features around channels 170 & 900.

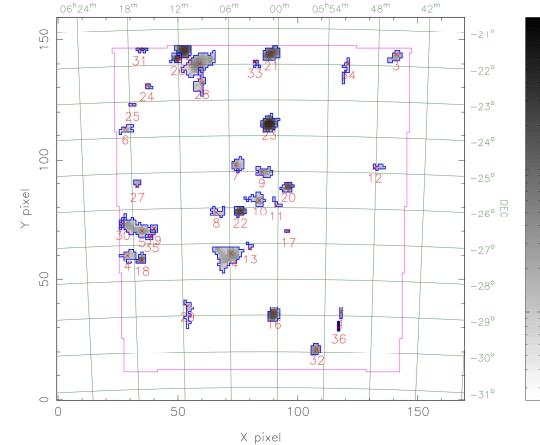


Figure 2: Example graphical output of *Duchamp* showing the zeroth moment of each detection, in its appropriate spatial location. This is provided as a postscript file and displayed in a PGPLOT window.

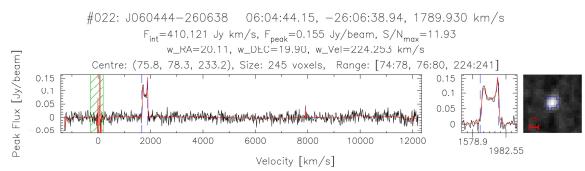


Figure 3: Example graphical output showing the spectral nature, the zeroth moment and the basic properties of a detection. A postscript file is produced showing such a plot for each object.

Obj#	Name	X	Y	Z	R.A.	DEC	VEL	w_VEL	u_VEL	v_VEL	F_int	F_peak	S/Near	X1	X2	Y1	Y2	Z1	Z2	Npix	Flag
1	J060356-263338	110.0	35.8	73.6	06:03:56.54	-26:33:38.94	-323,477	5.58	26,10	52,765	5,131	0,125	5,115 115	34	38	9	74	11	11	11	E
2	J060356-263338	110.0	35.8	73.6	06:03:56.53	-26:33:38.94	-323,477	5.58	26,10	52,765	5,131	0,125	5,115 115	34	38	9	74	11	11	11	E
3	J064456-214408	84.9	145.9	144.7	06:44:56.03	-21:44:08.96	-227,293	23.52	20,78	25,381	46,146	0,095	6,33 138	141 141	145 145	114 115	33	33	33	33	E
4	J064456-214408	84.9	145.9	144.7	06:44:56.03	-21:44:08.96	-227,293	23.52	20,78	25,381	46,146	0,095	6,33 138	141 141	145 145	114 115	33	33	33	33	E
5	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
6	J063827-234057	26.6	112.6	115.6	06:38:27.08	-23:40:57.08	-274,274	24.51	15,25	25,383	10,399	0,070	5,38 20	31 311	114 115	117 117	21	21	21	21	E
7	J063827-234057	26.6	112.6	115.6	06:38:27.08	-23:40:57.08	-274,274	24.51	15,25	25,383	10,399	0,070	5,38 20	31 311	114 115	117 117	21	21	21	21	E
8	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
9	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
10	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
11	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
12	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
13	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
14	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
15	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
16	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
17	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
18	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
19	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
20	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
21	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
22	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
23	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
24	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
25	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
26	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
27	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
28	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
29	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
30	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
31	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
32	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
33	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
34	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
35	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
36	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
37	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148	712,333	0,117	9,64 115	110 110	110 110	110 110	110	110	110	110	E
38	J061738-263327	32.6	154.8	154.8	06:17.38	-26:33:27.07	-226,625	61.04	30,20	93,148											