

Tracing Pumping Routes in OH

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Understanding OH Pumping

- Analytic estimates backed by numerics^{34 152}
- Inferences from parameter-space searches
- Thermodynamic schemes¹⁰
- Monte-Carlo technique used on water masers¹¹
- Analogy with currents + Monte-Carlo on methanol¹²
- How do we manage ‘complexity’?
- Problem not confined to maser studies

Elitzur et al.³, Elitzur⁴, Bujarrabal et al.¹, Sobolev¹⁰, Elitzur⁵, Dickinson², Sobolev¹¹, Sobolev & Deguchi¹²

Population Tracing

- RT solutions from numerical method (e.g. LU-factorization)
- Numerical results (level populations, mean intensities) are computed, but much physical insight lost
- The code TRACER restores population transfer information.
- A converged model is re-solved by the naive method
- Coefficient $k_{x,y}^z$ now has a simple interpretation:
- ...rate coefficient for transfer of population from level x to level y with z eliminations to go.

An Example

- Choose $x = 2$, $y = 10$ and $z = 16$.
- Look at modification to next elimination, $z = 15$.
- $k_{2,10}^{15} = k_{2,10}^{16} + k_{2,15}^{16} k_{15,10}^{16} / k_{15,15}^{16}$
- Begin at small value of z and work back
- Eventually expand to coefficients with $z = N + 1$:
 N is the number of energy levels in model.
- No guarantee of simplicity!

Additional Detail

- Start from a small matrix (e.g. 3×3).
- Solve for inversion in required line.
- Organise rate-coefficients: antagonistic pairs
- ‘Direct’ and ‘Indirect’ parts of pump
- Begin computer analysis with TRACER
- Reduce all rate coefficients to unmodified form.

The 1612 MHz Inversion

- The formula for the 1612 MHz inversion, at $z = 4$ is
-

$$\Delta\rho_{32} = \frac{\mathcal{N}k_{1,2}^4}{D} \left\{ (1 + \eta) \left(\frac{k_{2,3}^4}{3} - \frac{k_{3,2}^4}{5} \right) + \frac{\eta k_{2,1}^4}{3} - \frac{k_{3,1}^4}{5} \right\}$$

- ...where $\eta = k_{1,3}^4/k_{1,2}^4$
- First part is 'direct pump'
- Second part gives 'indirect' pump via level 1:

Other Ground-State Inversions

$$\Delta\rho_{31} = \frac{Nk_{2,2}^4}{3D} \left\{ k_{1,3}^4 - k_{3,1}^4 + \left(\frac{k_{1,2}^4 k_{2,3}^4 - k_{3,2}^4 k_{2,1}^4}{k_{2,2}^4} \right) \right\}$$

$$\Delta\rho_{42} = \frac{N'}{5} \left\{ k_{2,4}^5 - k_{4,2}^5 + \frac{k_{1,1}^5}{X} (k_{2,3}^5 k_{3,4}^5 - k_{4,3}^5 k_{3,2}^5) + \frac{k_{3,3}^5}{X} (k_{2,1}^5 k_{1,4}^5 - k_{4,1}^5 k_{1,2}^5) \right. \\ \left. + \frac{k_{2,1}^5 k_{1,3}^5 k_{3,4}^5 - k_{4,3}^5 k_{3,1}^5 k_{1,2}^5}{X} + \frac{k_{2,3}^5 k_{3,1}^5 k_{1,4}^5 - k_{4,1}^5 k_{1,3}^5 k_{3,2}^5}{X} \right\}$$

$$\Delta\rho_{41} = N' \left\{ \frac{k_{1,4}^5}{5} - \frac{k_{4,1}^5}{3} + \frac{k_{3,3}^5}{X} \left(\frac{k_{1,2}^5 k_{2,4}^5}{5} - \frac{k_{4,2}^5 k_{2,1}^5}{3} \right) + \frac{k_{2,2}^5}{X} \left(\frac{k_{1,3}^5 k_{3,4}^5}{5} - \frac{k_{4,3}^5 k_{3,1}^5}{3} \right) \right. \\ \left. + \frac{k_{1,2}^5 k_{2,3}^5 k_{3,4}^5}{5X} - \frac{k_{4,3}^5 k_{3,2}^5 k_{2,1}^5}{3X} + \frac{k_{1,3}^5 k_{3,2}^5 k_{2,4}^5}{5X} - \frac{k_{4,2}^5 k_{2,3}^5 k_{3,1}^5}{3X} \right\}$$

Example Pump Traces

- 1612 MHz in a detached Mira envelope - study of envelope detachment; time dependence
- 1612 and 1667 MHz in a larger envelope (M-type supergiant); 35 micron lines
- 1665 MHz for typical star-forming region
- 1667 MHz (conditions as for 1665)

1612 MHz Inversion

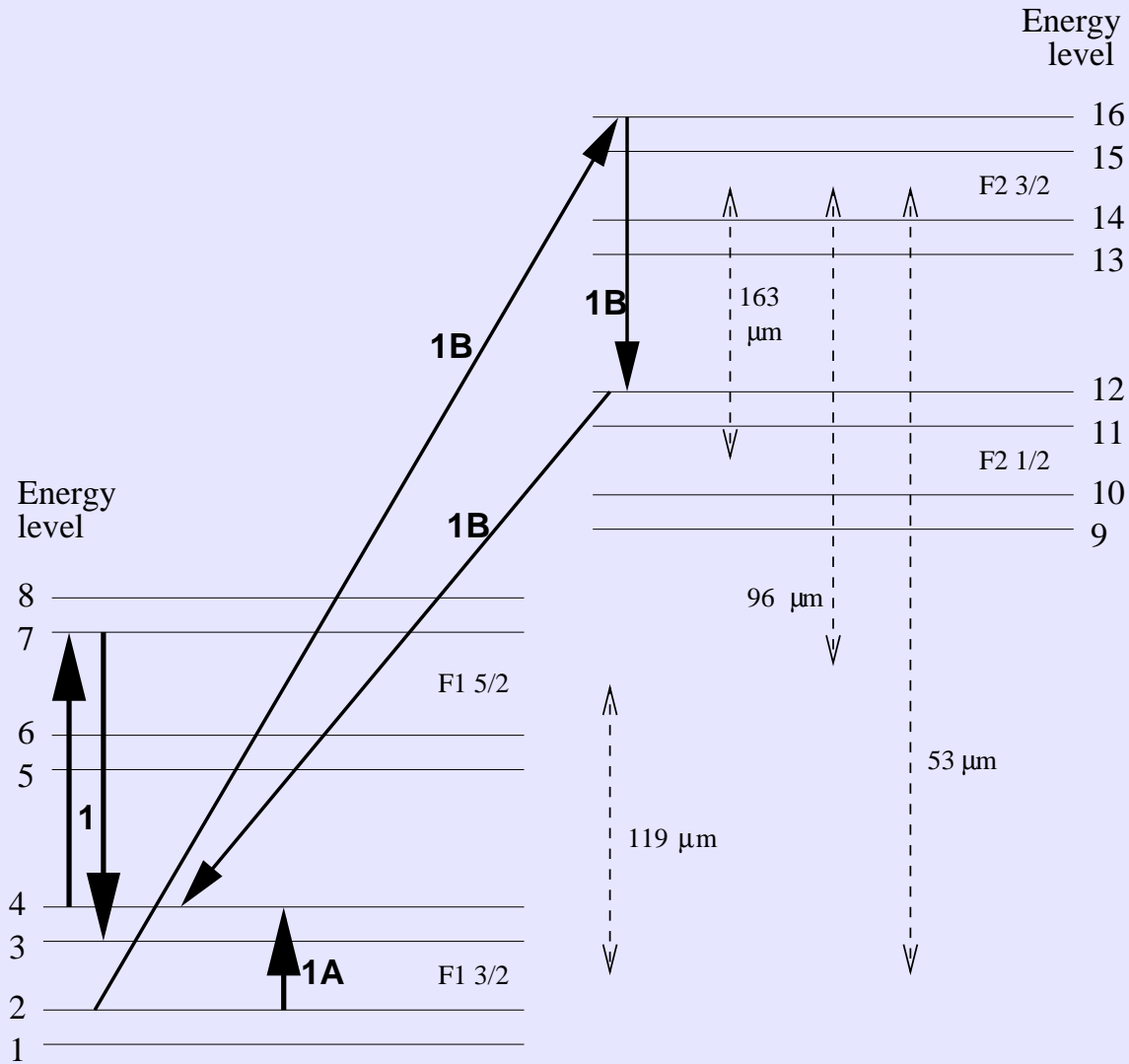
- Formula for indirect pump:

$$\frac{1}{k_{1,2}^4} \left[\left(\frac{k_{2,1}^4}{3} \right) k_{1,3}^4 - k_{3,1}^4 \left(\frac{k_{1,2}^4}{5} \right) \right]$$

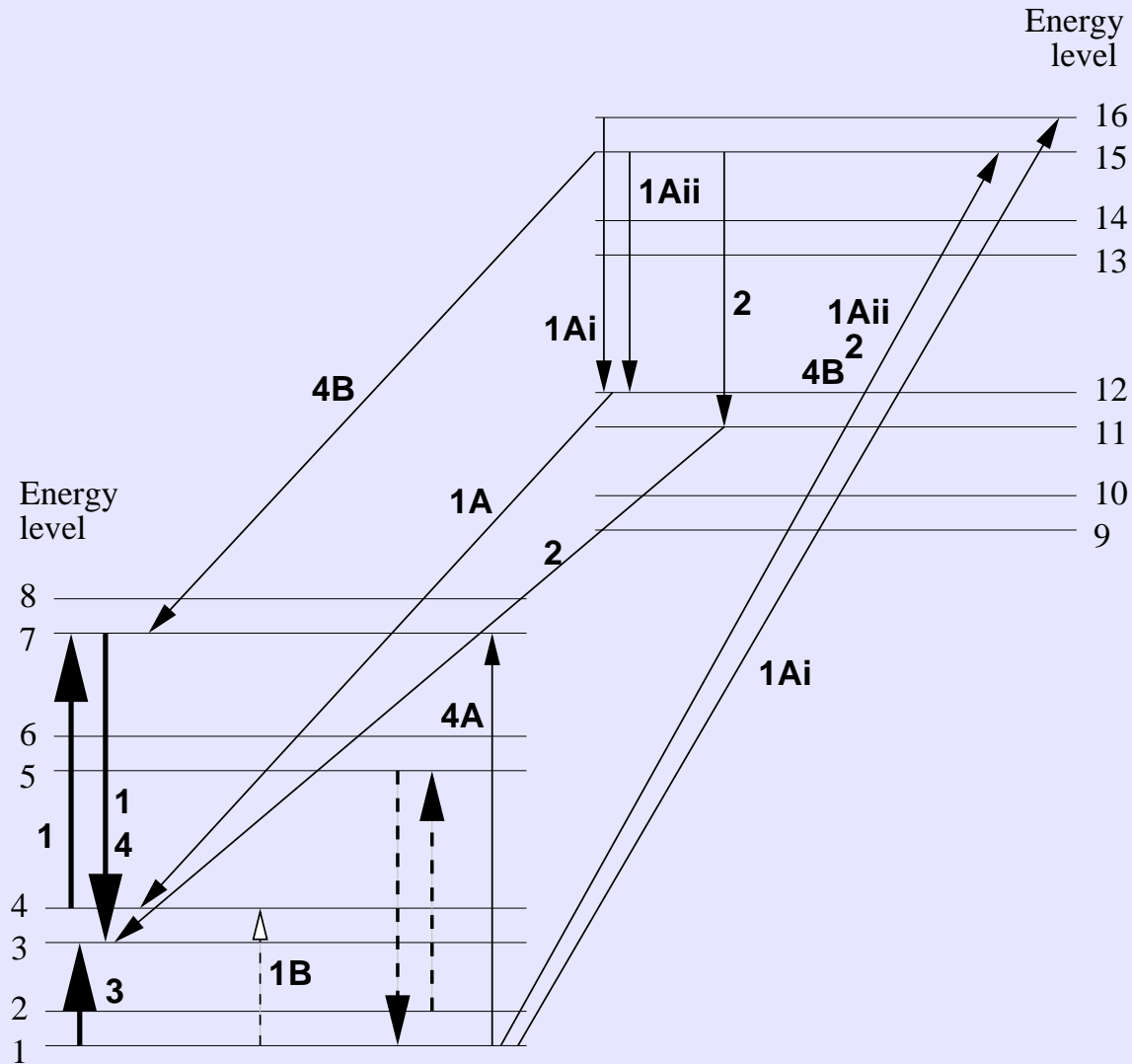
- At shell detachment, 2/3 of pump is 'direct'
- Most of loss of gain 40 yr later due to collapse of *indirect* pump.
- Publication of results (2005)⁷

Gray et al.⁷

Diagram: Routes of the Direct Pump



Routes for the Indirect Pump



Summary

- Most important radiative pump uses $53\ \mu\text{m}$ radiation.
- Routes via level 1 more dependent on $53\ \mu\text{m}$ photons.
- Expanding detached shell cools.
- $53\ \mu\text{m}$ energy density reduces with time.
- Vulnerable part of pump (via level 1) collapses
- 1612 MHz line in absorption ~ 50 yr after detachment.

1612/65 MHz: Larger Envelope

- Model of M supergiant
- 35 micron radiation important
- model based on S Per (M4.5)
- 1612 MHz pump more like traditional scheme³
- 1665 MHz pump (shown) returns without ${}^2\Pi_{1/2}, J = 1/2$ to ${}^2\Pi_{3/2}, J = 3/2$
- strongest routes in black (then green, purple)

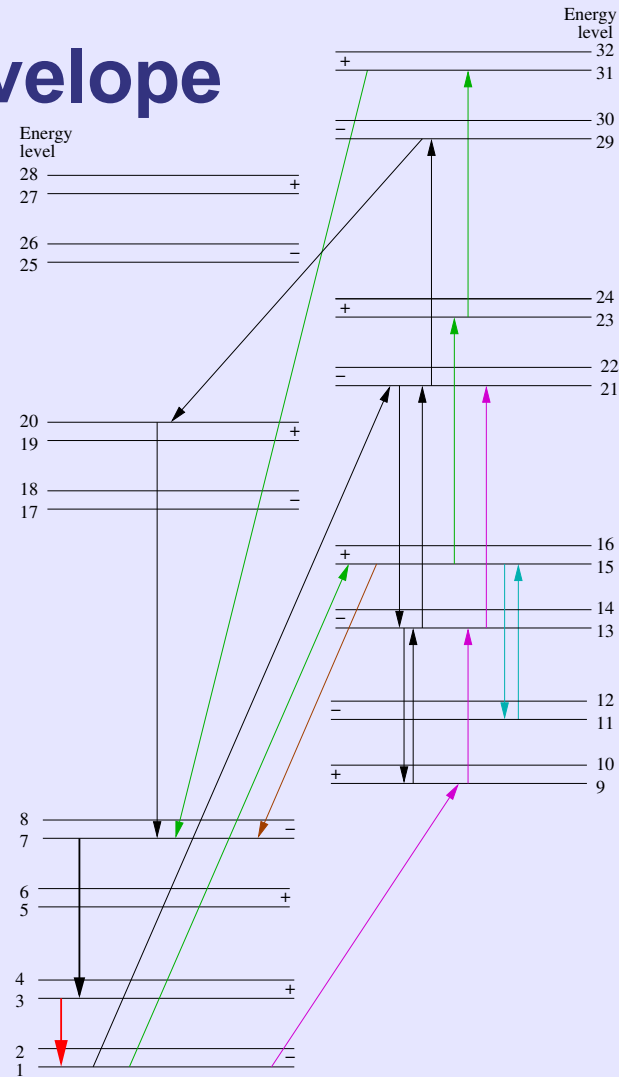
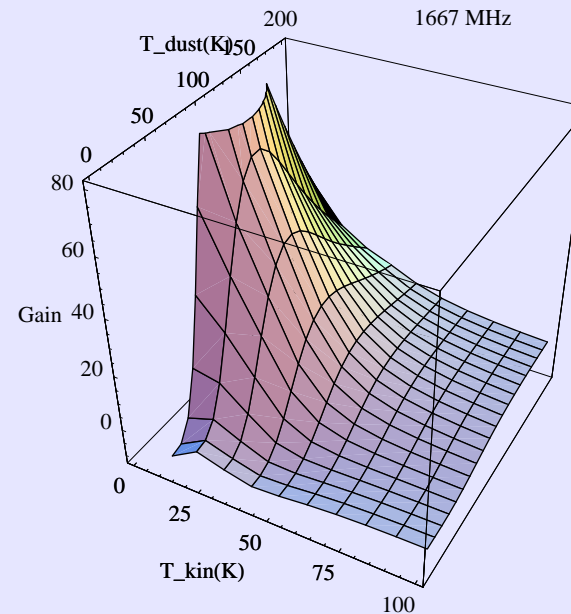
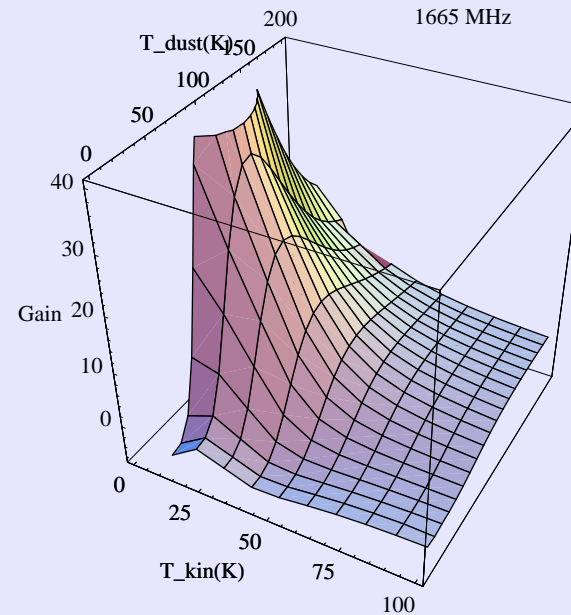


Figure 1: Pump routes for 1665 MHz in an M-supergiant

Elitzur et al.³

Star-Forming Regions

- Model: part of parameter-space search
- Slab ALI solution with strong main-line inversions:
- 48 levels, conditions as follows:
 - 80 log-spaced depths in 2×10^{13} m
 - $n_{H_2} = 10^7 \text{ cm}^{-3}$; $[\text{OH}] = 0.2 \text{ ppm}$
 - $T_K = 30 \text{ K}$; $T_d = 70 \text{ K}$
 - no microturbulence; no velocity gradient
 - unsaturated integrated gains: 20.039 at 1665 MHz; 35.661 at 1667 MHz



1665 MHz Trace

- (i) $k_{1,3}^4 - k_{3,1}^4 = 1.05 \times 10^{-4} \text{ s}^{-1}$
- (ii) $(k_{1,2}^4 k_{2,3}^4 - k_{3,2}^4 k_{2,1}^4) / k_{2,2}^4 = 9.07 \times 10^{-5} \text{ s}^{-1}$
- Two dominant routes in (i) supply 83% of it.
- Three dominant routes in (ii) supply 80.5% of it.
- These break down to a set providing 82% of the total:
 - (i) $(k_{1,5}^6 k_{5,3}^6 - k_{3,5}^6 k_{5,1}^6) / k_{5,5}^6 = 6.01 \times 10^{-5} \text{ s}^{-1}$
 - (ii) $(k_{1,5}^6 k_{5,2}^6 k_{2,4}^6 k_{4,3}^6 - k_{3,4}^6 k_{4,2}^6 k_{2,5}^6 k_{5,1}^6) / (k_{2,2}^4 k_{4,4}^5 k_{5,5}^6) = 4.86 \times 10^{-5} \text{ s}^{-1}$
 - (iii) $(k_{1,4}^5 k_{4,3}^5 - k_{3,4}^5 k_{4,1}^5) / k_{4,4}^5 = 2.72 \times 10^{-5} \text{ s}^{-1}$
 - (iv) two further terms totalling $2.46 \times 10^{-5} \text{ s}^{-1}$

Further Complexity

- Route (i) has no additional complexity!
- Route(ii) very complex but 3 routes control 73% of it:
 - (A) a route via levels 4, 6 and 7;
 - (B) a route via level 20 (in F1, $J=7/2$);
 - (C) via levels 10 and 14 (visits F2, $J=1/2$ & $3/2$)
- Route (iii) is worse still: top 3 routes comprise 50%:
 - (A) web of routes via 9, 10, 14 and 20;
 - (B) a route via 10 and 14, excluding level 9;
 - (C) a route involving a collisional transfer from $4 \rightarrow 3$

1665 MHz Pump

- the most important route
- energy levels not to scale
- pump entirely in F1
- upward step radiative
- downward step collisional
- reverse routes not shown

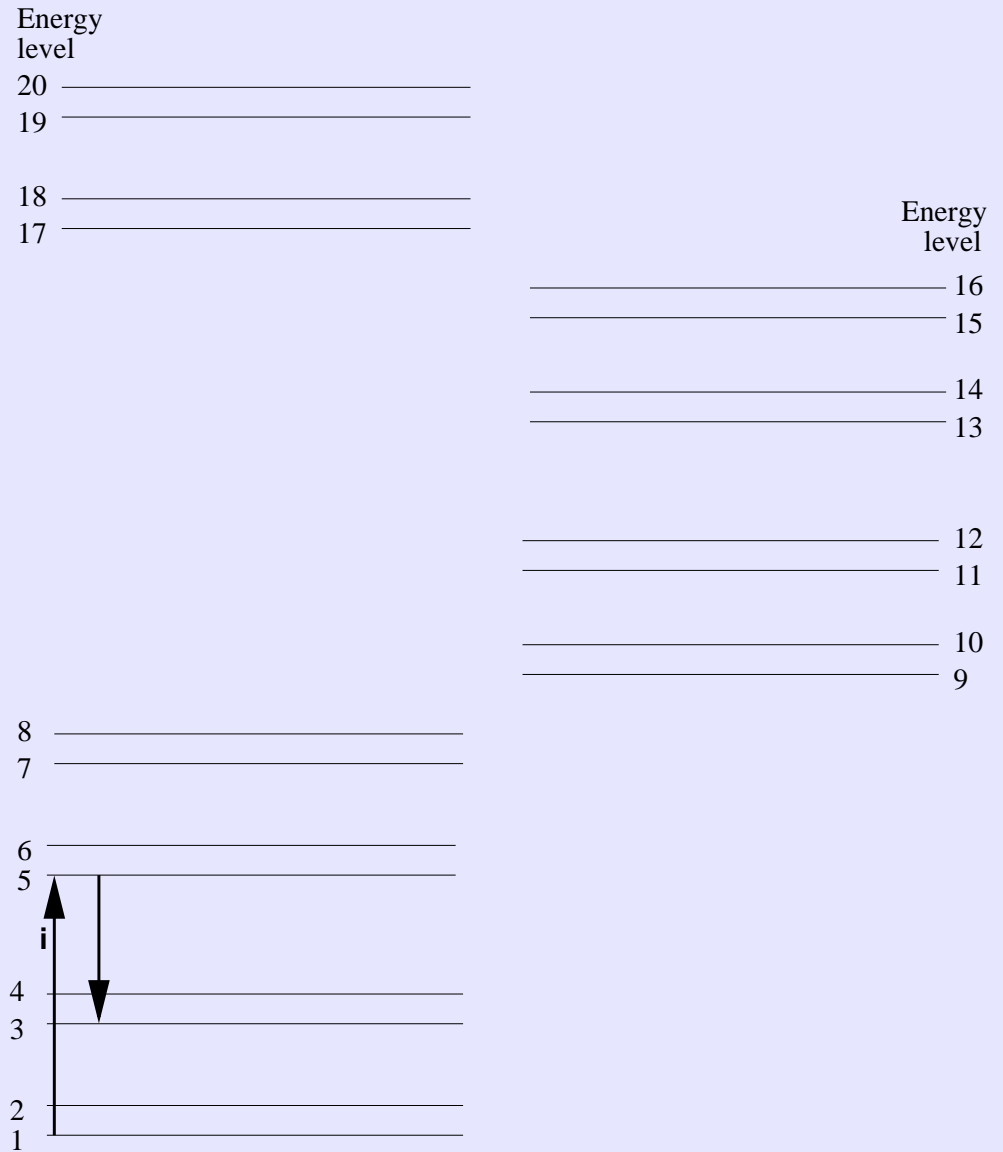


Figure 3: Strongest Pump Routes at 1665 MHz

1665 MHz Pump

- the two most important routes
- energy levels not to scale
- pump predominantly in F1
- mostly radiative steps
- some collisional steps, e.g. $5 \rightarrow 3$ and $6 \rightarrow 4$
- upward routes only shown

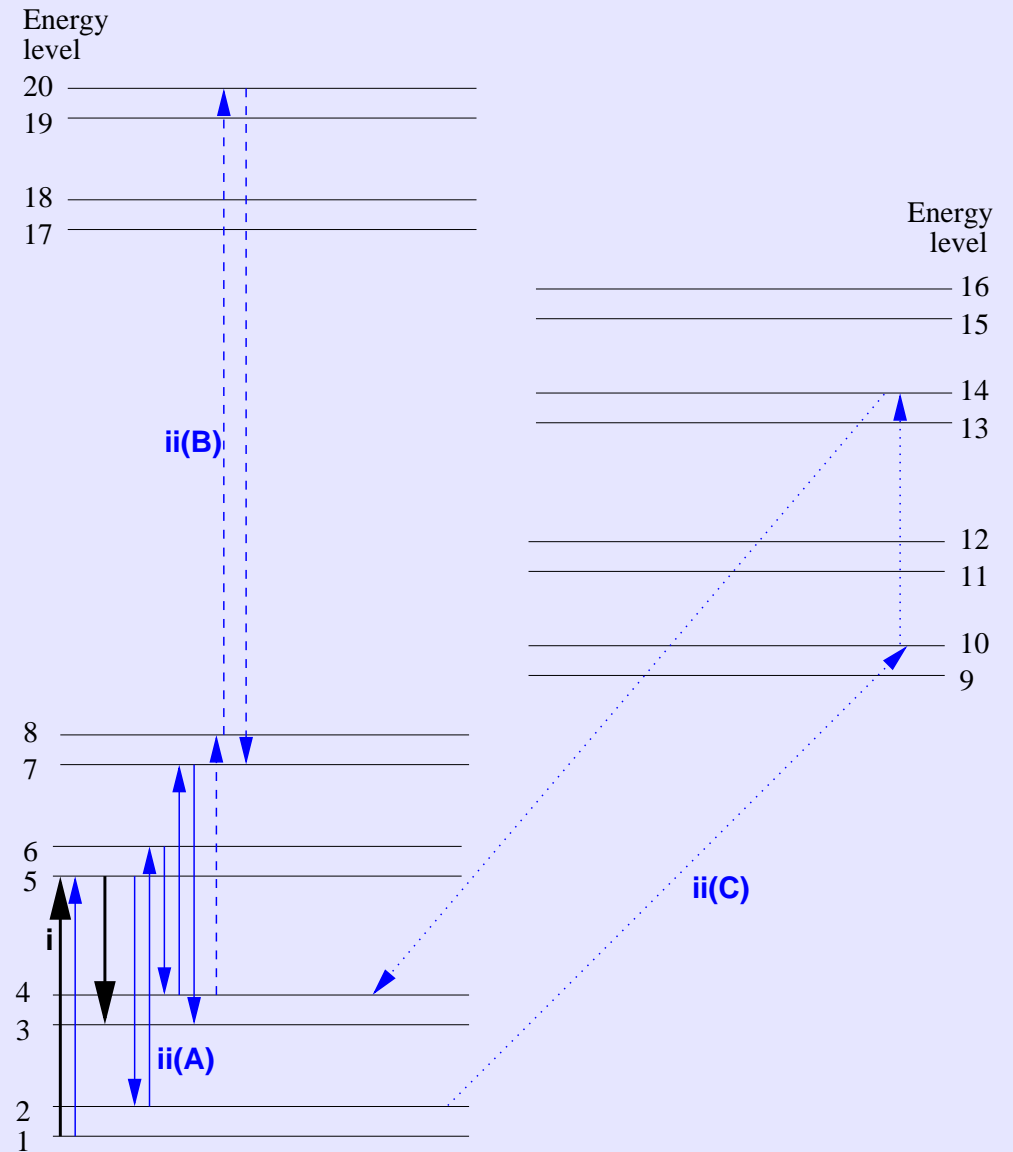


Figure 4: Strongest Pump Routes at 1665 MHz

1665 MHz Pump

- 3 most important routes
- energy levels not to scale
- pump predominantly in F1 BUT
- route iii uses F2 stack a lot
- mostly radiative
- several important collisional links
- upward routes only shown

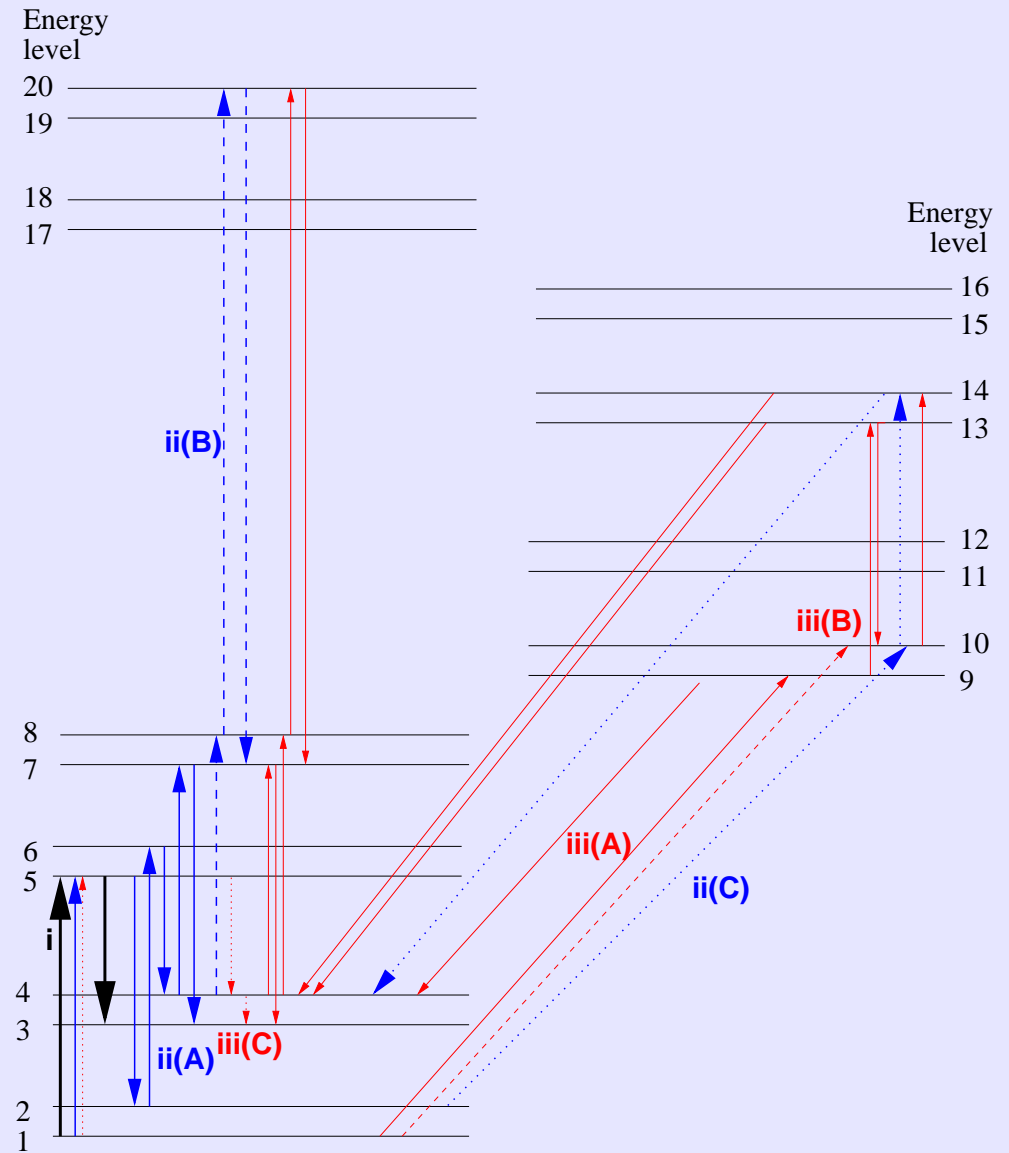


Figure 5: Strongest Pump Routes at 1665 MHz

1667 MHz Pump

- relative strengths:
- i = 1.0
- ii = 0.413
- iii = 0.290
- iv = 0.255
- v = 0.228
- vi = 0.203
- vii = 0.112

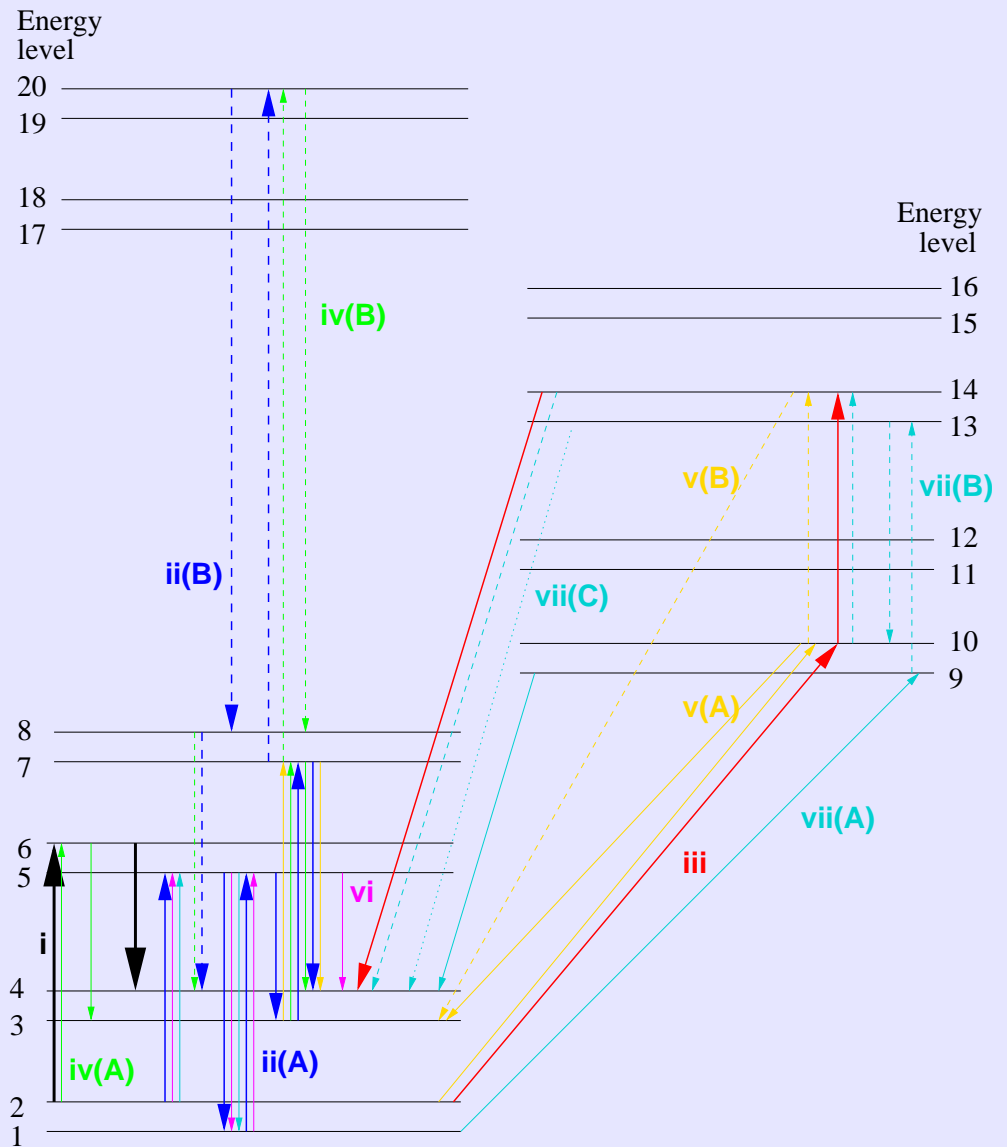


Figure 6: Strongest Pump Routes at 1667 MHz

1665 and 1667 Compared

- Detailed results now published ⁶
- Pumps share many features.
- Routes in F1 stack are dominant
- Strongest route goes only to F1, $J=5/2$
- $1 \rightarrow 5 + 5 \rightarrow 3$ in 1665; $2 \rightarrow 6 + 6 \rightarrow 4$ in 1667
- radiative 'up'; collisional 'down'
- Weaker routes use F2 stack much more.

Gray ⁶

At a Deeper Level

- Expand rate coefficients: radiative & collisional parts
- Example: strongest 1665 MHz pump
- $k_{1,5}k_{5,3} - k_{3,5}k_{5,1}$ expands as:

$$[B_{1,5}\bar{J}_{1,5} + C_{1,5}]C_{5,3} - C_{3,5}[A_{5,1} + B_{5,1}\bar{J}_{1,5} + C_{5,1}]$$

- Values in Hz: $C_{5,3} = 3.75(-4)$; $C_{3,5} = 1.13(-5)$
 $A_{5,1} = 0.1244$; $B_{5,1}\bar{J}_{1,5} = 2.160(-2)$; $C_{5,1} = 3.16(-4)$
 $B_{1,5}\bar{J}_{1,5} = 3.60(-2)$; $C_{1,5} = 9.48(-5)$
- Ignore cross-products of collision terms

What is Responsible?

- Also, $C_{5,3} \gg C_{3,5}$ (by a factor > 10) so,
- $k_{1,5}k_{5,3} - k_{3,5}k_{5,1} \sim B_{1,5}\bar{J}_{1,5}C_{5,3} - A_{5,1}C_{3,5}$
- Put B s and C s in terms of downward coefficients

$$k_{1,5}k_{5,3} - k_{3,5}k_{5,1} \sim (C_{5,3}g_5/g_1)[B_{5,1}\bar{J}_{1,5} - A_{5,1}e^{-\frac{h\nu}{kT_K}}]$$

$$= \frac{A_{5,1}C_{5,3}g_5/g_1}{e^{-\frac{h\nu}{kT_K}}} \left[\frac{\bar{J}_{1,5}}{B_\nu(T_K)} - 1 + e^{-\frac{h\nu}{kT_K}} \right]$$

- The exponential is $\ll 1$

The Answer?

- Multiplier is just a rate: says nothing about inversion
- $k_{1,5}k_{5,3} - k_{3,5}k_{5,1} \sim K((\bar{J}_{1,5}/B_\nu(T_K) - 1)$
- Inversion depends on two things:
 - (i) 3→5 energy gap large for T_K
 - favours $C_{5,3}$ over $C_{3,5}$.
 - (ii) Dust continuum (at $T_d = 70$ K) hotter than T_K
 - allows mean intensity $>$ black-body at T_K .

Digging Deeper Still

- Source of 70 K radiation is optically thick boundary
- Radiation diffusion approximation applicable here
- $\frac{\bar{J}_{1,5}}{B_\nu(T_K)} - 1 = \left[\frac{B_\nu(T_d)}{B_\nu(T_K)} - 1 \right] e^{-\sqrt{3}\zeta(\tau_M - \tau)}$
- scattering parameter ζ modifies optical depth
- value $\zeta \sim C_{5,1}/A_{5,1} = 3.51(-4)$
- Radiation is not thermalised

Parity Propensity

- Why do 'mirror routes' not cancel inverting effects?
- Example: route linking levels 3 and 1 via 7 (instead of 5)
- $C_{7,1}$ is considerably smaller than $C_{5,3}$
- $C_{7,1}$ not leading term in TRACER expansion
- Contribution from collisions with para-hydrogen is explanation
- Parity propensity disappears at temperatures above 100 K
- no propensity in OH + ortho- H_2

Future Plans

- Additional scenarios: SNR 1720 MHz; megamasers
- How typical are these pumps?
- Increase automation
- Role of velocity gradients
- Extend method to other molecules: H₂O in progress
- Extend method to excited states
- Other problems reducible to pseudo-linear algebra

Conclusions

- Expanding all-process rate-coefficients can reveal pump routes
- Routes can be separated into inverting and anti-inverting sets.
- For ‘dying’ OH-IR stars decay of gain is mainly caused by changes to the routes operating via level 1
- Larger, ‘supergiant’, envelopes rely more on 35 micron radiation
- In star-forming regions, main-line pump is mainly radiative but with crucial collisional steps.

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