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# Continuum observations

## Total Intensity and Polarisation

Ettore Carretti  
Systems Scientist: Parkes Observatory  
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# What are continuum observations meant for?

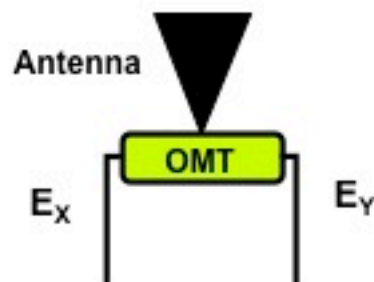
- To measure the bulk of the radio emission
  - energy density content
  - spectral behaviour
  - understanding emission processes
  - understanding object physics
- Synchrotron emission
- Free-free emission
- Thermal emission: starbursts galaxies (high freq: 20+ GHz)
- high sensitivity (broadband)
- faintest radio sources

# Radiometer offset

- The total power signal is the auto-correlation of each polarisations.

$$I = XX^* + YY^*$$

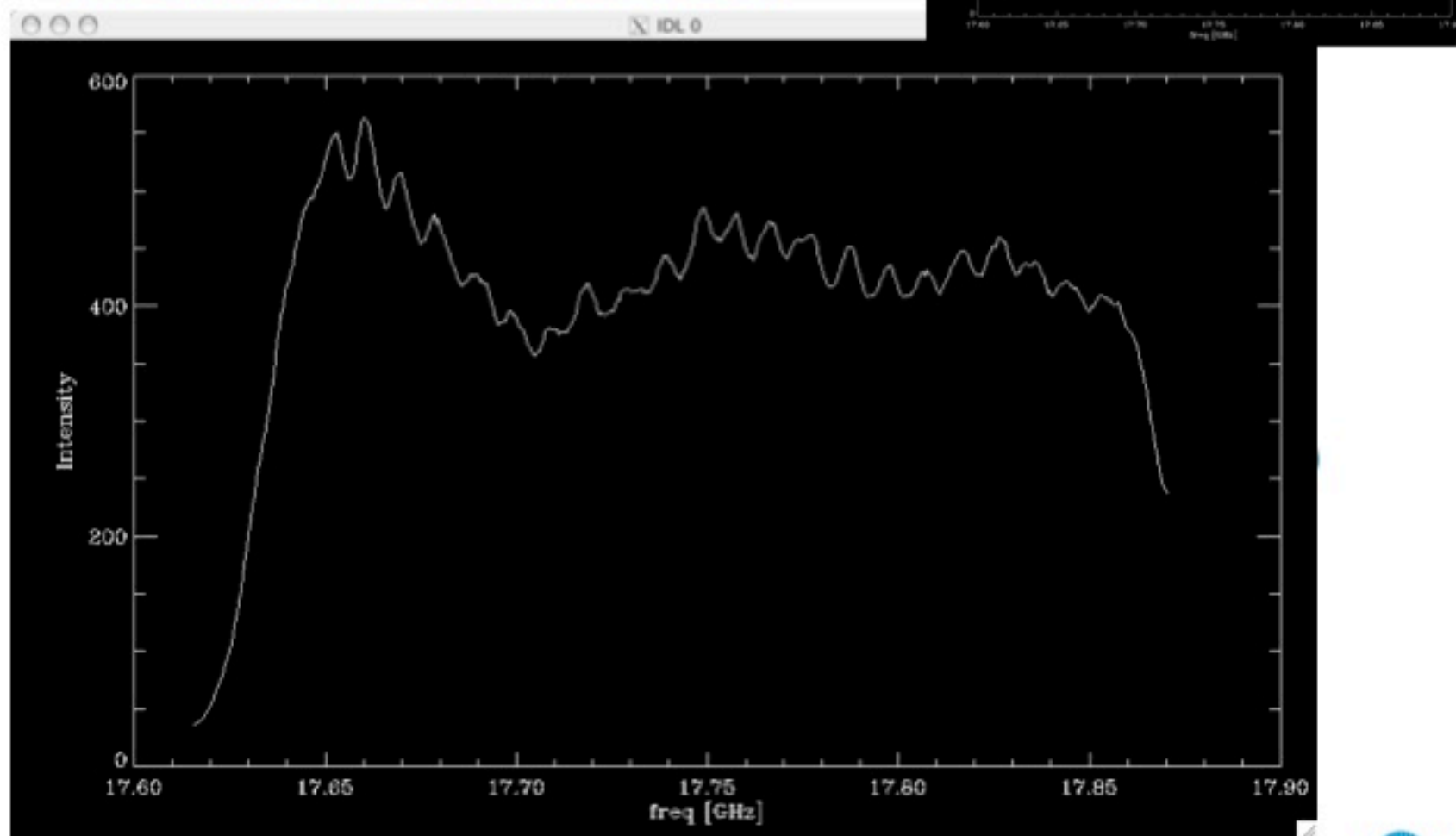
$$I = LL^* + RR^*$$



- Autocorrelation: also the noise is detected.

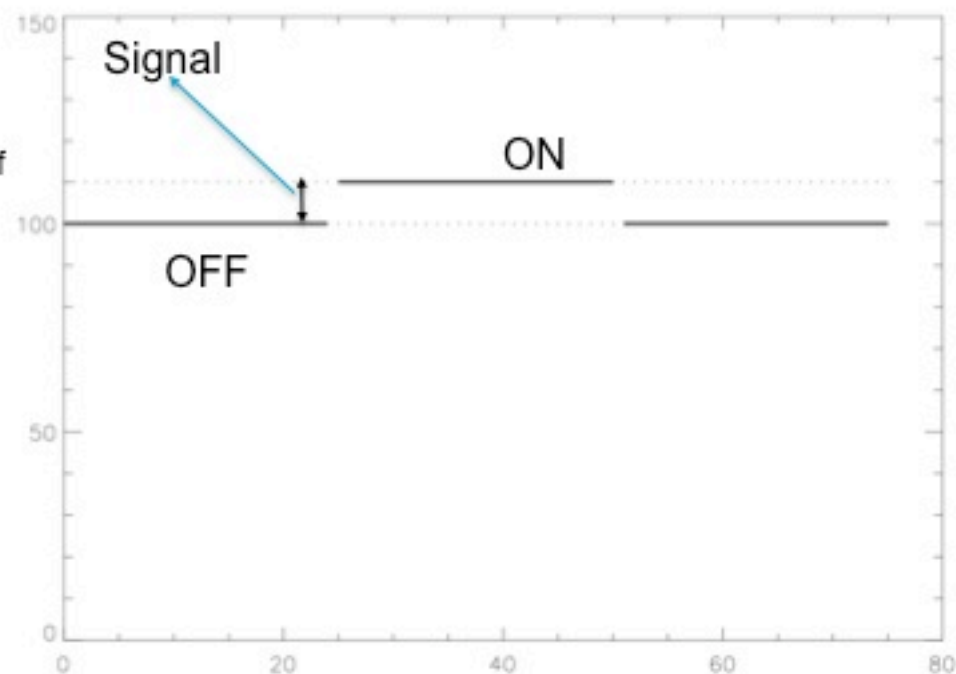
# Radiometer offset

- The total power signal is non-zero.



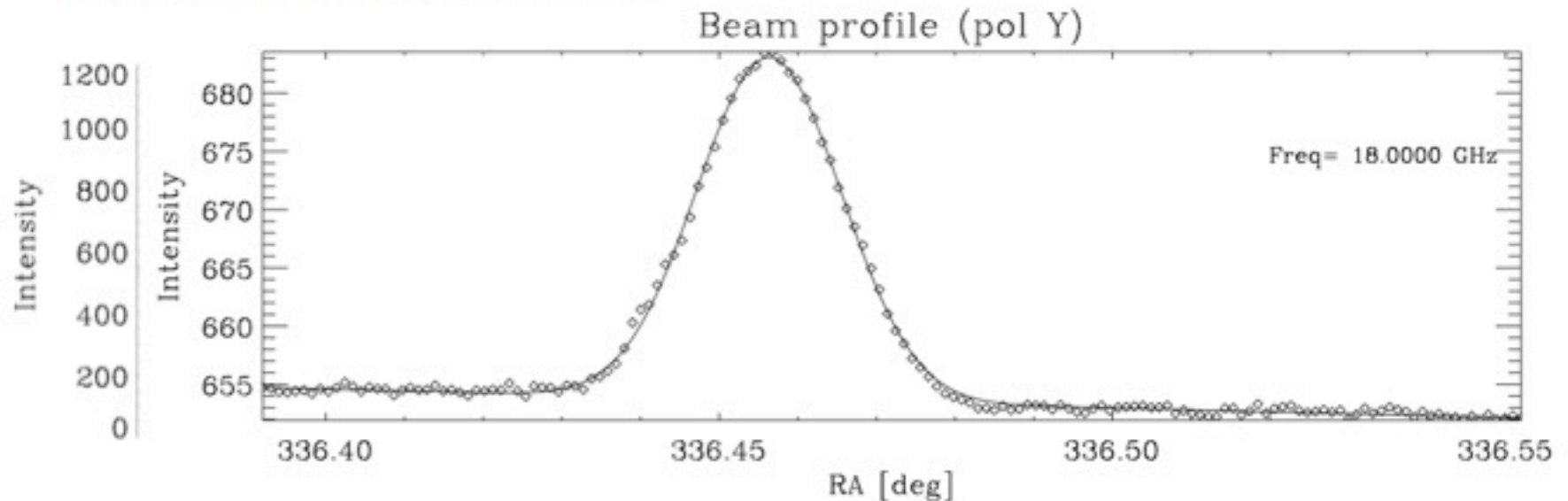
# Signal-offset separation

- **Position switching**
- It consists of at least two observations, one on-source, one off-source. The radiometer offset is common, and the subtraction gives the source signal:
  - off-source  $\Rightarrow S_1 = S_{\text{off}}$
  - on-source  $\Rightarrow S_2 = S_{\text{src}} + S_{\text{off}}$
- $S_{\text{src}} = S_2 - S_1$
- Atmospheric emission can depend on Elevation (EL)
  - preferred off position: AZ



# Signal-offset separation

- On-The-Fly scanning (OTF)
- scan through the source
- fitting with beam shape (Gaussian) + polynomial baseline (linear) allows to separate source from offset/background emission.
- linear => variations with EL



# Sensitivity Equation

- Receiver Sensitivity Equation:

$$\sigma = k \frac{T_{sys}}{\sqrt{BW * \tau}}$$

- BW = bandwidth
  - $\tau$  = integration time
  - $k \sim 1$  (depends on the receiver architecture type.  $k=1$  for TI)
- $T_{sys} \Rightarrow$  quality of the receiver (LNAs, cryo, reflector, feed IL)
  - BW  $\Rightarrow$  the broader, the better  $\Rightarrow$  continuum observations

# Integration Time

$$\sigma = k \frac{T_{sys}}{\sqrt{BW * \tau}}$$

- $\tau \Rightarrow$  long integration time, better sensitivity
- Is it true?
- Is long integration time always good?

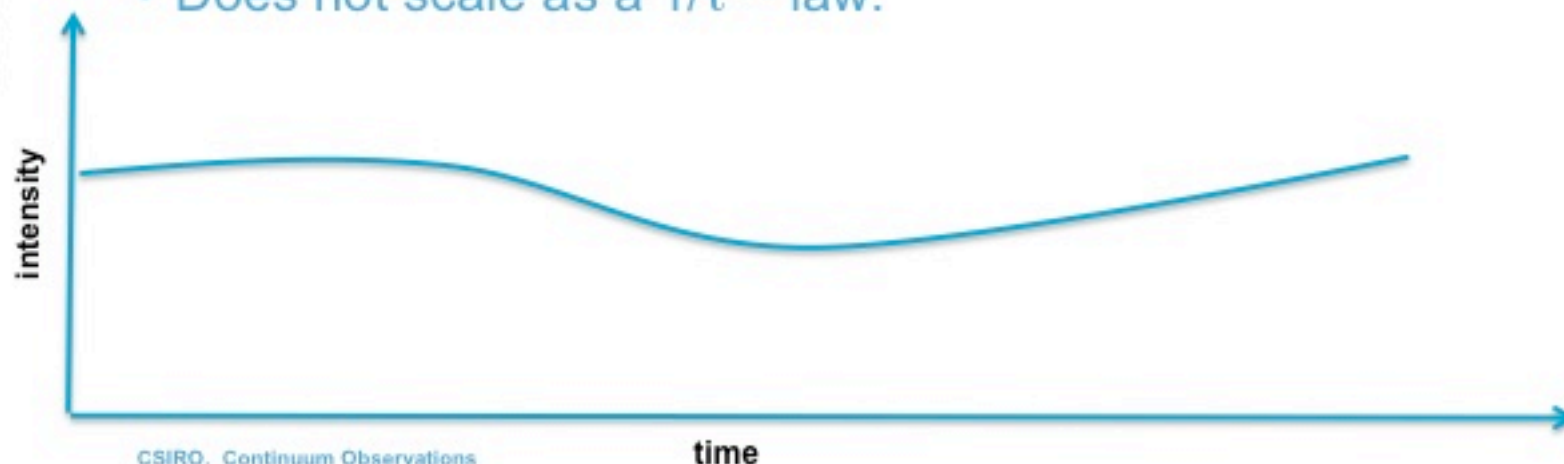


# Real Sensitivity Equation

- Amplifiers (LNA) are active components => Gain fluctuations

$$\sigma = k * T_{sys} \sqrt{\frac{1}{BW * \tau} + \left( \frac{T_{off}}{T_{sys}} \frac{\Delta G}{G} \right)^2}$$

- Additional noise  $\Delta G/G$ :  
1/f noise (after its spectral properties).  
 $T_{off} = T_{sys}$  (for total intensity)
- Does not scale as a  $1/\tau^{1/2}$  law.



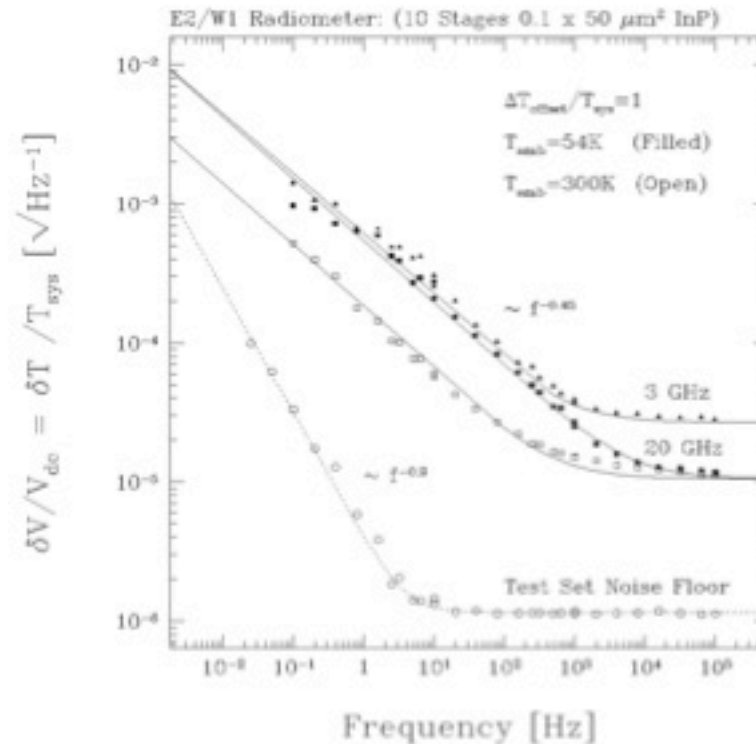
# Gain Fluctuations

- Total Intensity observations have offsets, signal which is generated either internally or collected by the telescope:
  - internal noise (i.e.  $T_{\text{sys}}$ , either LNA noise or feed system)
  - atmosphere
  - ground emission
  - background emission (e.g., CMB  $\Rightarrow$  3K)
- it runs from  $\sim 20\text{K}$  (e.g. L-band MB-20) to  $\sim 200\text{K}$  (e.g. 90GHz)
- Gain fluctuations of active components (e.g. LNAs) make this background to vary: even small fluctuations of a 20+ K background can jeopardise detection of  $\sim \text{mK}$  signals.
- it is particularly important for Continuum obs (high sensitivity required)

# 1/f noise

- noise spectrum (receiver detected output)
  - Normal (ideal) white noise has flat spectrum:  $P(f) = \sigma_0^2$
  - $\sigma_0^2 =$  sensitivity for integration time of 1 sec
  - Gain fluctuations add a steep inverted component  $P(f) \propto 1/f$
- Total spectrum:

$$P(f) = \sigma_0^2 \left( 1 + \frac{f_{knee}}{f} \right)$$



# 1/f noise

- Total spectrum:

$$P(f) = \sigma_0^2 \left( 1 + \frac{f_{knee}}{f} \right)$$

- key parameter  $\Rightarrow f_{knee} \Rightarrow 1/f$  equals white noise
- $\tau_{knee} = 1/f_{knee} \Rightarrow$  transition time between the two ranges

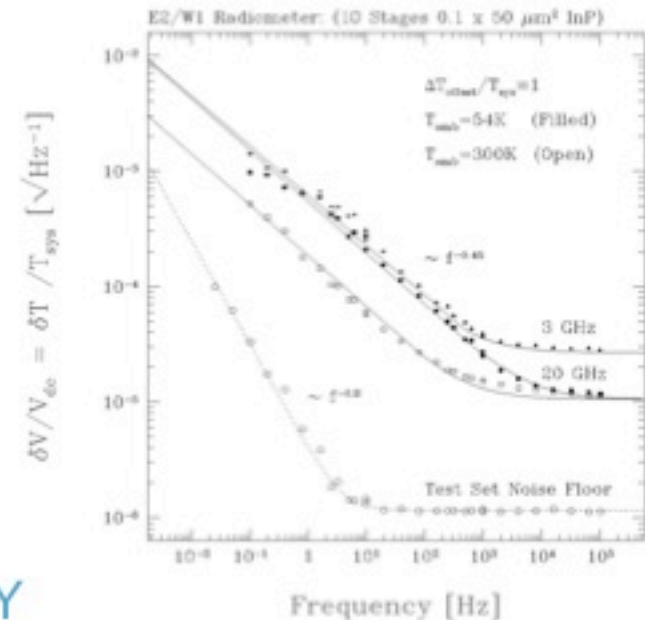
- sensitivity:

$$\sigma^2(\tau = 1/f) \approx f * P(f)$$

- white noise:  $\sigma_{wn}^2 \approx \sigma_0^2 * f \approx \sigma_0^2 / \tau$

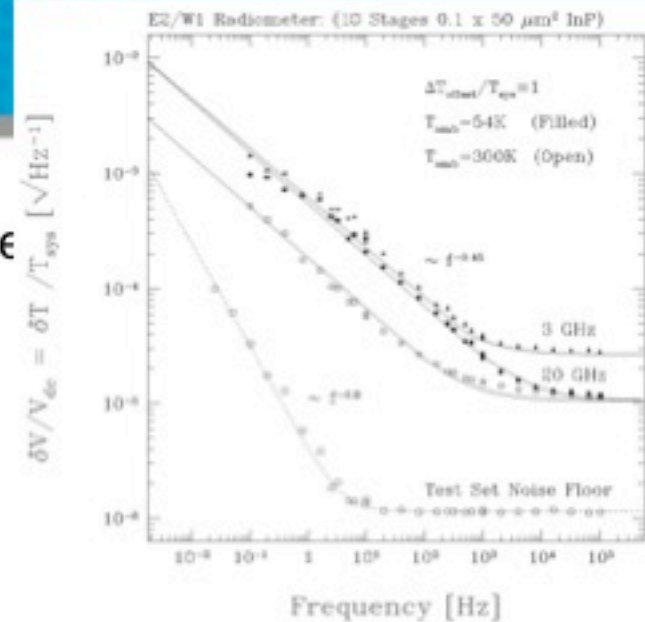
- 1/f noise:  $\sigma_{1/f}^2 \propto f / f = const$

- for  $\tau < 1/f_{knee} \Rightarrow$  NO GAIN IN SENSITIVITY

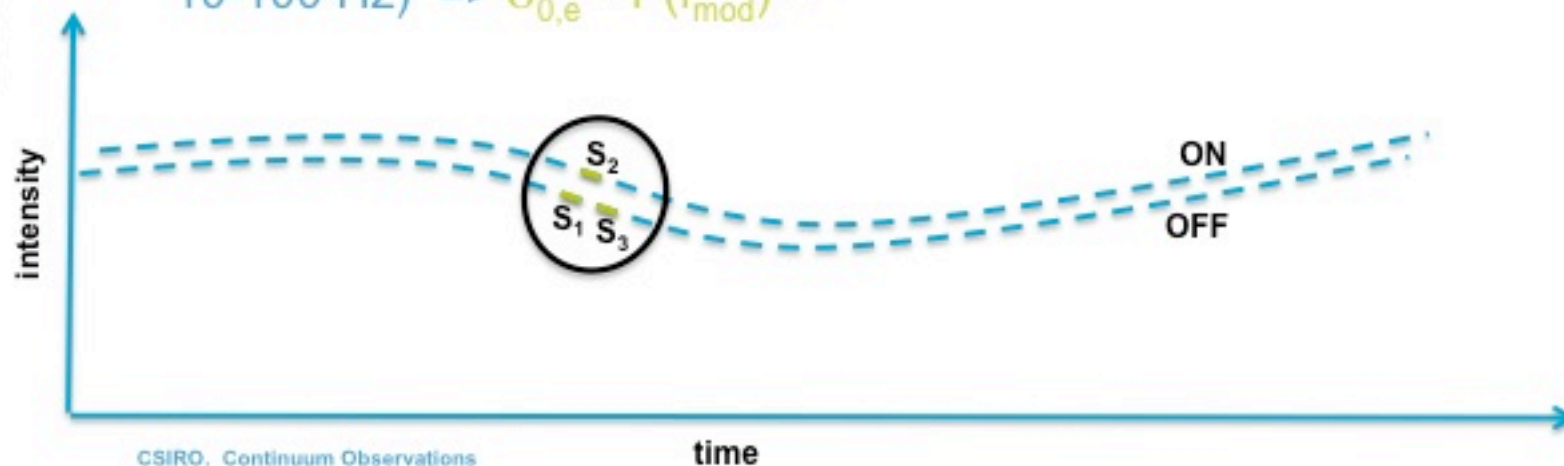


# Position Switching

- if position-switching period  $\tau_{\text{mod}} < 1/f_{\text{knee}} \Rightarrow$ 
  - ON and OFF have same behaviour and the
  - Most effective a three way procedure
    - pre off-source  $\Rightarrow S_1 = S_{\text{off}}$
    - on-source  $\Rightarrow S_2 = S_{\text{src}} + S_{\text{off}}$
    - post off-source  $\Rightarrow S_3 = S_{\text{off}}$
    - $S_{\text{src}} = S_2 - (S_1 + S_3)/2$

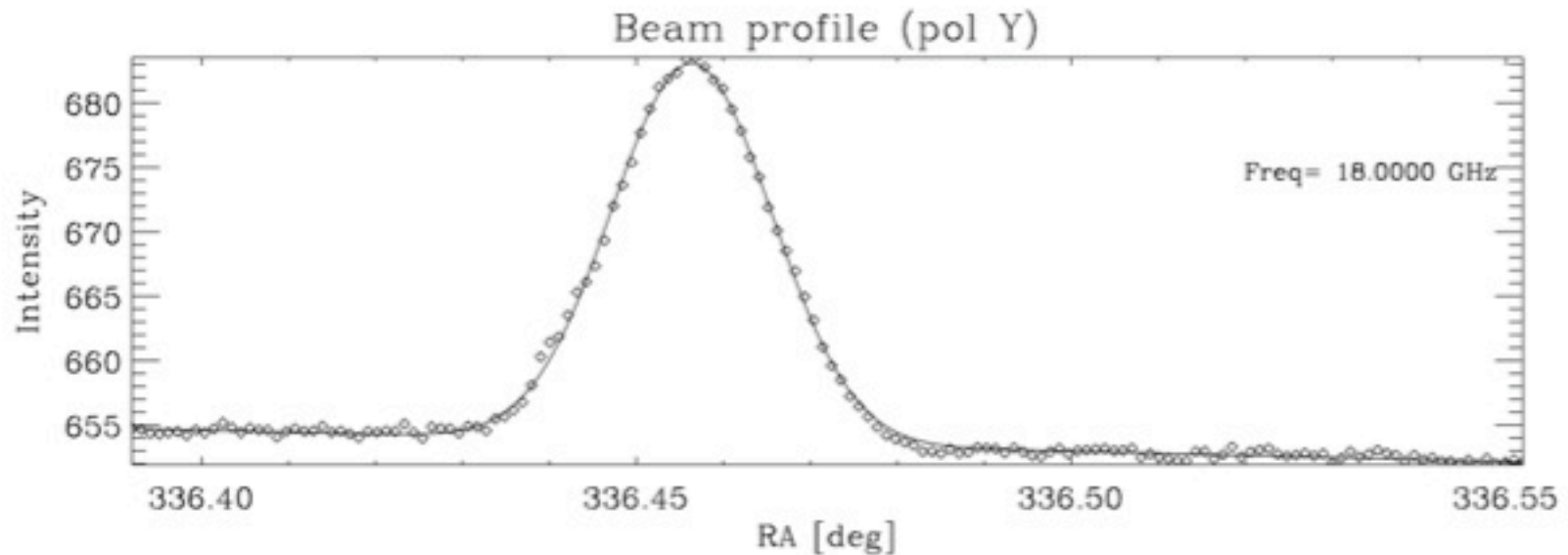


- Sensitivity worsen by a factor 2 (reasonable cost)
- typical scale 1-min: marginally effective for current systems ( $f_{\text{knee}} \sim 10\text{-}100\text{ Hz}$ )  $\Rightarrow \sigma_{0,e} \sim P(f_{\text{mod}})^{1/2}$



# source scanning

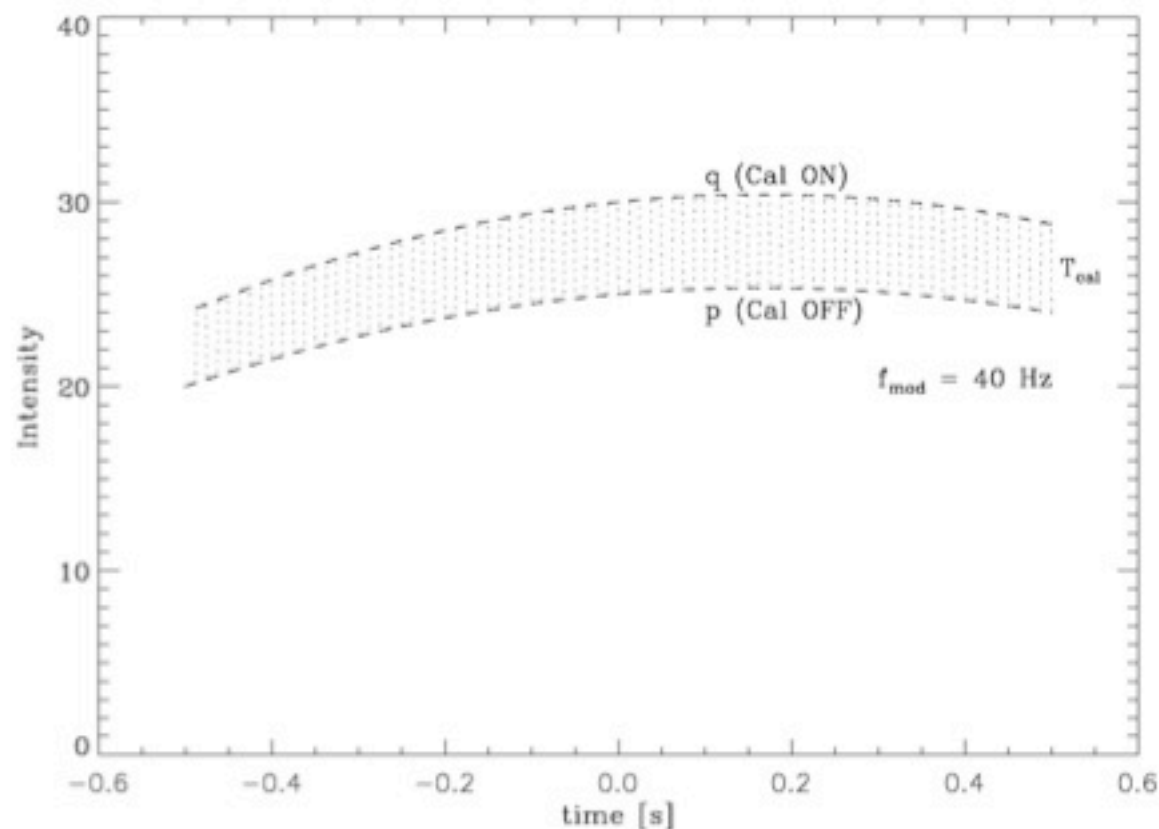
- baseline fitting allows accounting for the Gain fluctuations
- $\tau_{\text{mod}}$  similar to pos. switch. (slow method)
- same issue:  $\sigma_{0,e} \sim P(f_{\text{mod}})^{1/2}$



# Gain rectification by Calibration signal modulation (1)

- measuring the gain by **modulating the signal**: periodically firing a known calibrated signal with sufficient time resolution ( $\tau_{\text{mod}} < \tau_{\text{knee}}$ ).
- rectifying the data
  - calibrated signal

$$S = \frac{T_{\text{cal}}}{q - p} p$$



# Gain rectification by Calibration signal modulation (2)

- Requirements:
- high frequency cal modulation:
  - $\tau_{\text{mod}} < \tau_{\text{knee}} \Rightarrow$  typical: ~10-100 Hz
  - at feed level and firing signal modulated with a pin-diode switch

- increased noise  $\sigma_{\text{cal}} = 2\sigma \frac{\sqrt{1 + f + f^2/2}}{f}$

$$f = \frac{T_{\text{cal}}}{T_{\text{sys}}}$$

- example

- $T_{\text{sys}} = 20\text{K}$
- $T_{\text{cal}} = 1\text{K}$
- $f \ll 1 \Rightarrow$

$$\sigma_{\text{cal}} \approx \frac{2}{f} \sigma \quad \Rightarrow \quad \sigma_{\text{cal}} \approx 40\sigma$$

- high cal signal

$$f = \frac{T_{\text{cal}}}{T_{\text{sys}}} \geq 1$$

$$\left\{ \begin{array}{l} f=1 \Rightarrow \sigma_{\text{cal}} = \sqrt{10} \cdot \sigma \\ f \gg 1 \Rightarrow \sigma_{\text{cal}} = \sqrt{2} \cdot \sigma \end{array} \right.$$

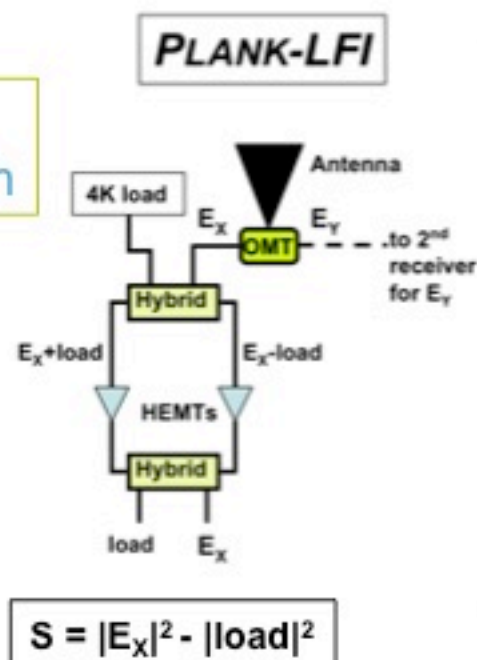


# Pseudo-correlation

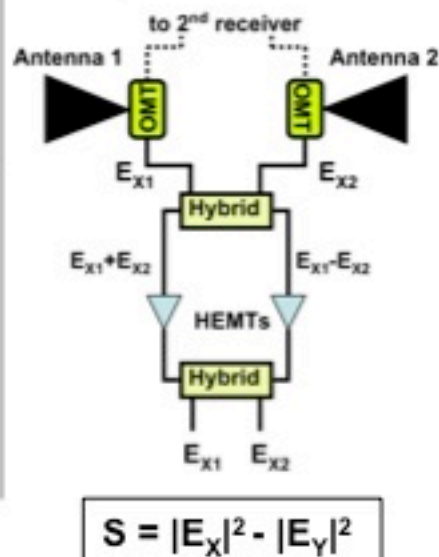
$$\sigma = k * T_{sys} \sqrt{\frac{1}{BW * \tau} + \left( \frac{T_{off}}{T_{sys}} \frac{\Delta G}{G} \right)^2}$$

- Receiver architectures to reduce offset:

Pseudo-correlation



**WMAP**



Differential

# Polarisation(1)

- Polarisation continuum observations are better suited
- Correlated outputs.
- Linear polarisation receiver

$$Q = |X|^2 - |Y|^2$$

$$U = \Re(XY^*)$$

$$V = \Im(XY^*)$$

- Q is a total power output => 1/f noise
- Not ideal for linear pol observations (Stokes Q & U)

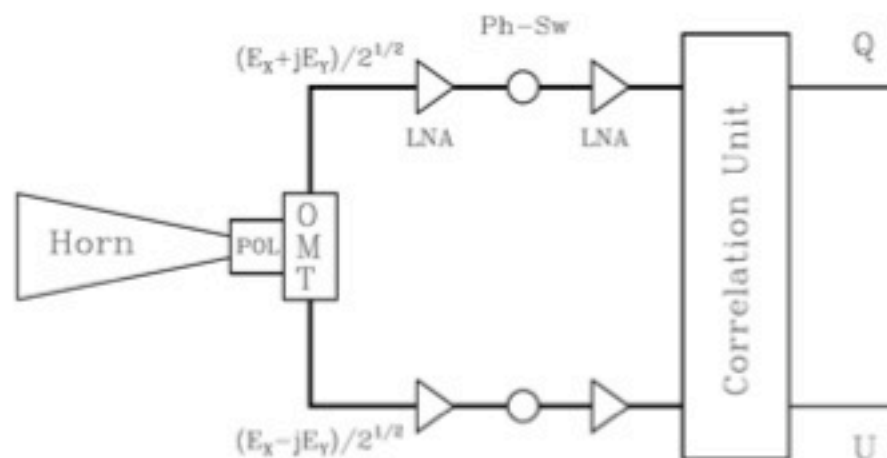
## Polarisation(2)

- Circular polarisation receiver:

$$Q = \Re(RL^*)$$

$$U = \Im(RL^*)$$

$$V = |R|^2 - |L|^2$$



# Polarisation: cross-correlation

- How does cross-correlation reduce the 1/f noise?

$$Q = \Re(RL^*)$$

$$U = \Im(RL^*)$$

$$V = |R|^2 - |L|^2$$

- Noise generated by the two LNAs are uncorrelated
- Noise generated by the feed in the two polarisations is uncorrelated.
- Cross-correlation has virtually no-offset

$$\sigma = k * T_{sys} \sqrt{\frac{1}{BW * \tau} + \left( \frac{\cancel{T_{off}} \Delta G}{\cancel{T_{sys}} G} \right)^2}$$

- Circular pol receiver: ideal for linear pol observations (Q & U)

# Polarisation: Stokes V

- Linear pol receiver: ideal for Stokes V observations

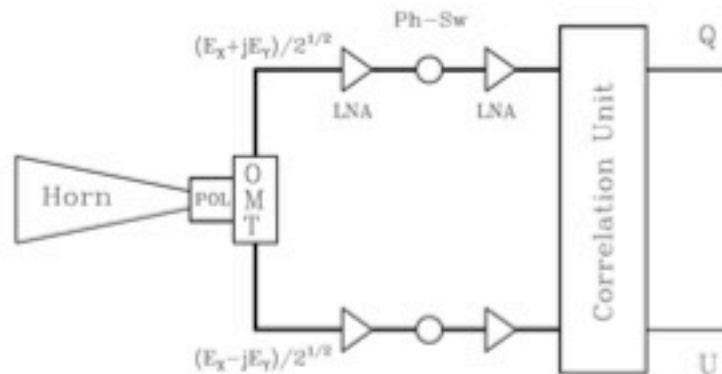
$$Q = |X|^2 - |Y|^2$$

$$U = \Re(XY^*)$$

$$V = \Im(XY^*)$$

# Instrumental Polarisation

- Zero offset is the ideal case
- **Leakages** between the two polarisations make the noise partly correlated.
- The unpolarised sky and ground emission too
- **Instrumental polarisation**
- However  $T_{\text{offset}} \ll T_{\text{sys}}$ : Correlation receiver is much more stable than a total power one.



## Instrumental Polarisation(2)

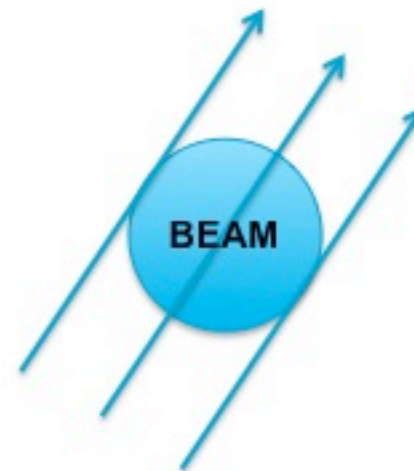
- How much more stable?

$$f_{knee} \propto \left( \frac{T_{off}}{T_{sys}} \right)^2$$

- instrumental pol P/I ~ 1%  $\Rightarrow f_{knee,pol} \sim 10^{-4} f_{knee,JP}$
- instrumental pol P/I ~ 3%  $\Rightarrow f_{knee,pol} \sim 10^{-3} f_{knee,JP}$
- $\Rightarrow \tau_{knee} \sim 100-1000s$
- usually sufficient for radioastronomical applications

# Mapping

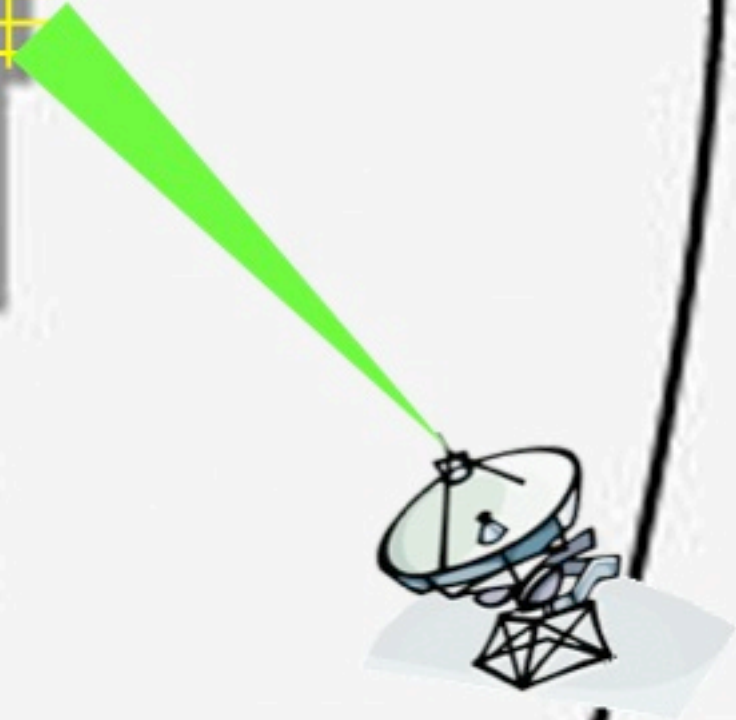
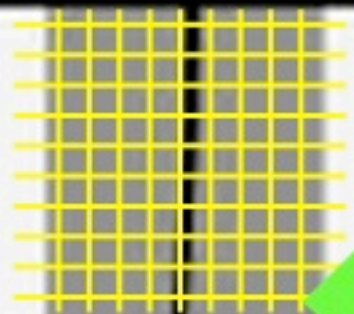
- 1 receiver => 1-pixel
- a few receivers, if you are lucky (e.g. Parkes Multi Beam 20cm)
- imaging is not an option (e.g., optical or interferometry)
- **mapping => scanning**
- area is mapped with a grid of scans spaced to ensure full sampling
  - 2+ scans per FWHM
  - 3 scans per beam is best



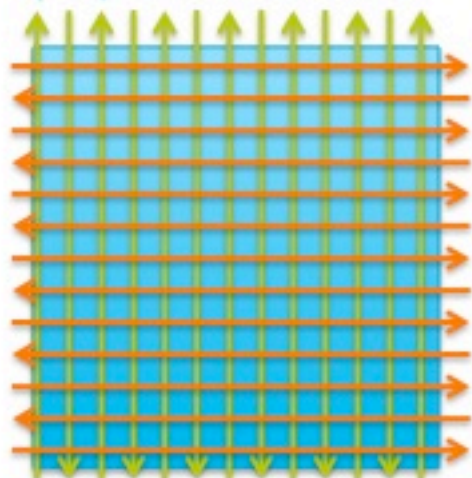


# The Parkes Galactic Meridian Survey (PGMS)

240°

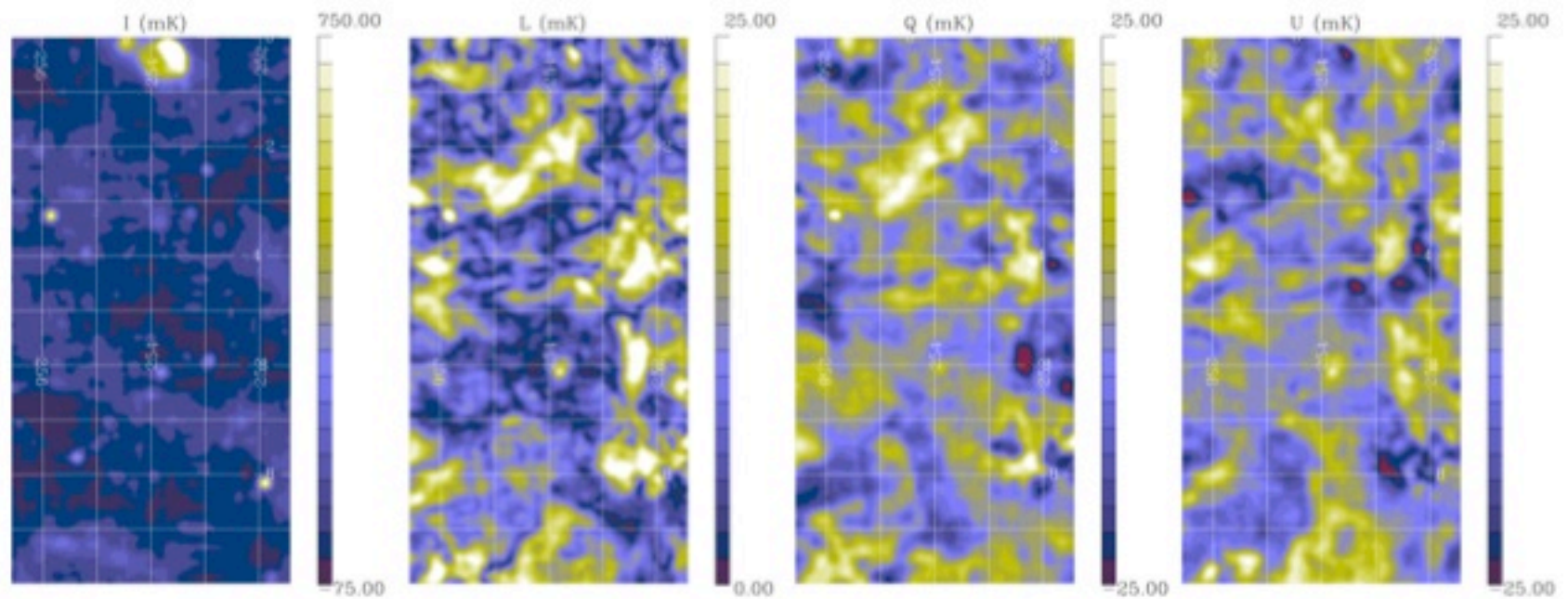


# Mapping

- offset: both for Total Intensity and Polarisation => baseline remove
  - Scans conducted in a Sky coordinate system (Equatorial, Galactic)
  - offset Variable with EL
  - linear baseline remove
    - loss of signal along the orthogonal direction
  - two full sets of scans along orthogonal directions (Basket-waving)
- 
- scan sets combined off-line to recover full-scale information
    - Fourier Methods (e.g., Emerson & Graeve 1988)
    - Destriping algorithms (e.g., Delabrouille 1998, Sbarra 2003)
  - Mean and gradient are lost (sufficient if area contains all the intended source)

# Mapping: examples

- Maps of the PGMS (Parkes Galactic Meridian Survey)

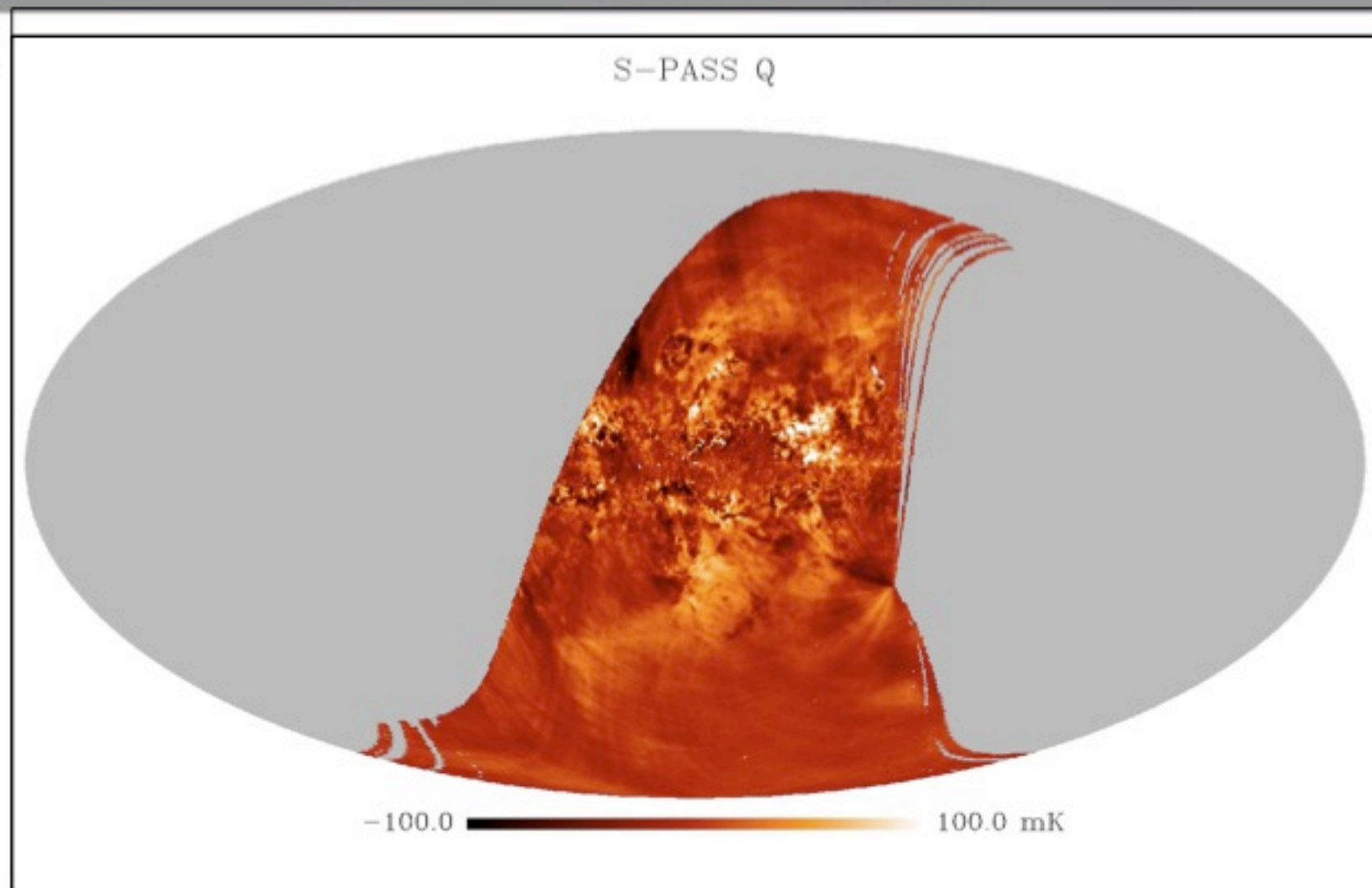


Carretti et al 2009

# Mapping: All-sky class surveys

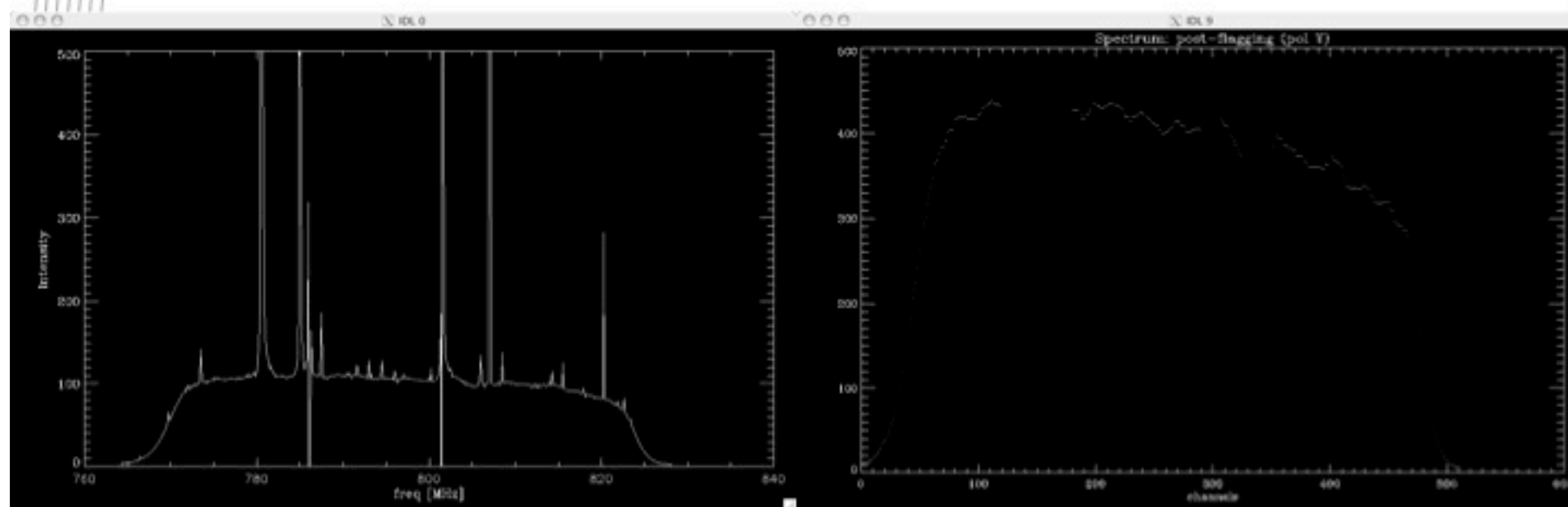
- All-sky class surveys:
- basket waving technique is an option
  - sky sub-divided in smaller areas then combined
- Most efficient are some **exotic/non-standard scanning strategies** (Not offered by all telescopes. Parkes does)
  - AZ (EL) scans.
  - Long AZ scans to cover all Dec in one haul
  - uses the Sky rotation to observe all RA 24 hrs. (Video)
  - each day/night a zig-zag track is observed in the sky
  - one zig-zag per night: accurate start timing is required

# Mapping: All-sky class surveys



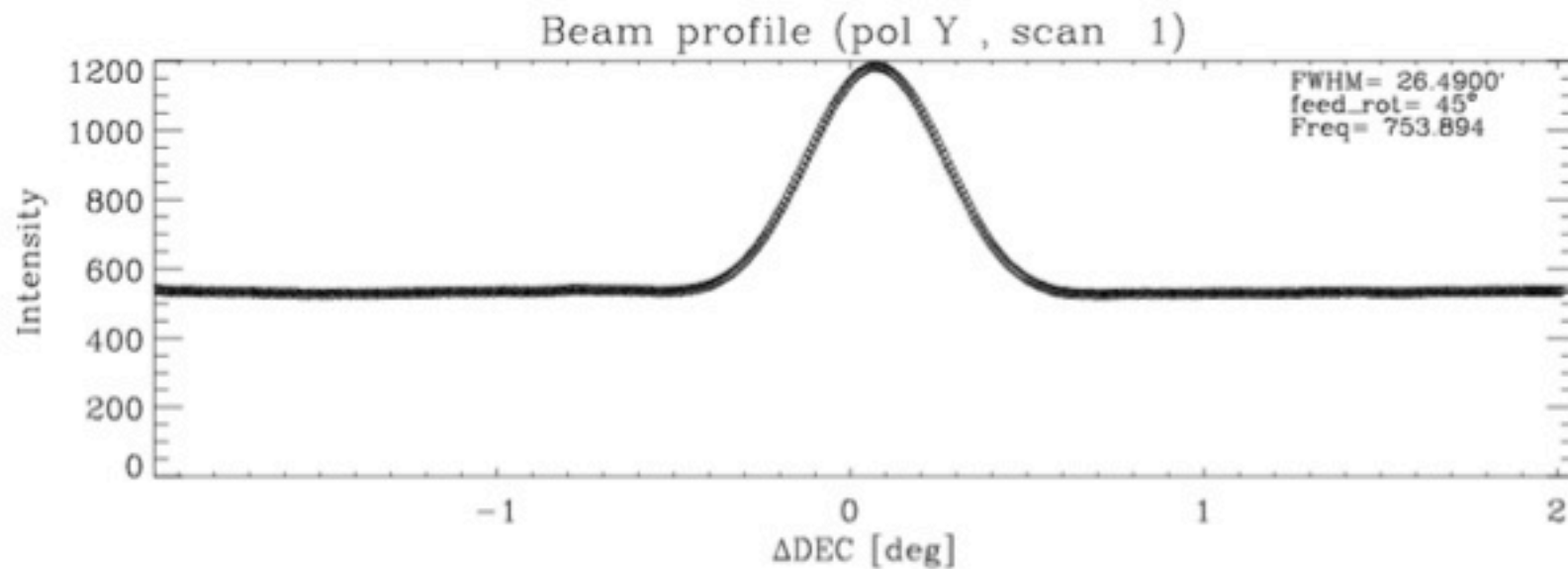
# Spectral observations

- Spectral observations with high frequency channel isolation (e.g. DFB3 => 65dB)
  - Strong RFI pollution => broad bands possible only flagging bad chan.
  - Spectral information + Rotation Measure (spectro-polarimetry)
- Now easily available with digital backends (Willem talk)



# Basics on Calibration: Flux

- Scan over a strong flux calibrated source
- To measure the gain  $K = \text{Jy}/\text{cnts}$



# Basics on Calibration: Instrumental polarisation

- Scan over an unpolarised source
- To measure the fractional polarised response:

$$f_Q = Q_{inst} / I$$

$$f_U = U_{inst} / I$$

$$f_V = V_{inst} / I$$

- To correct the measured data

$$Q = Q_m - f_Q I$$

$$U = U_m - f_U I$$

$$V = V_m - f_V I$$



# Basics on Calibration: polarisation angle

- Q and U measured as cross-product:

$$Q = \Re(RL^*)$$

$$U = \Im(RL^*)$$

- Any phase difference  $\phi$  add an instrumental pol angle
  - $\Delta\alpha = \phi/2$
- Scan over a polarisation calibration of intrinsic polarisation angle  $\alpha_0$  to measure the phase error
  - $\phi = \tan^{-1}(Q_m/U_m) - 2\alpha_0$
- Similar considerations hold for Stokes V (linear polarisations)

# Basics on Calibration: Mueller matrix

- Most complete calibration of polarisation leakages:

$$\begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix} = M \begin{pmatrix} I_m \\ Q_m \\ U_m \\ I_{Vm} \end{pmatrix}$$

- In case of the calibration described earlier:

$$M = \begin{pmatrix} 1 & 0 & 0 & 0 \\ f_Q & \cos(\phi/2) & \sin(\phi/2) & 0 \\ f_U & -\sin(\phi/2) & \cos(\phi/2) & 0 \\ f_V & 0 & 0 & 1 \end{pmatrix}$$

# Key points to plan a continuum obs

- **Offset:** to be estimated and removed
- **Total intensity:**  $1/f$  noise kills sensitivity => signal modulation
- **Polarisation:** correlation kills  $1/f$  noise => long integration times
- **Polarisation: chose receiver type according to what you need:**
  - Q & U => circular polarisation receiver
  - V => linear polarisation receiver
- **Mapping** => scanning (one or few receivers)
- **Calibrations** => flux and instrumental polarisation effects.

**ATNF Parkes Observatory**

Ettore Carretti

Senior Systems Scientist

Email: [Ettore.Carretti@csiro.au](mailto:Ettore.Carretti@csiro.au)

Web: [www.atnf.csiro.au](http://www.atnf.csiro.au)

[www.csiro.au](http://www.csiro.au)

Thank you