

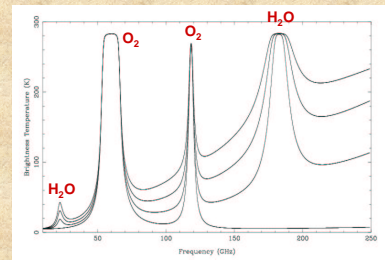
## Techniques for Millimetre Interferometry



Tony Wong, ATNF  
Synthesis School  
2001

## The trouble with mm-waves

- More stringent instrumental requirements
- Phase fluctuations due to H<sub>2</sub>O in troposphere
- Tropospheric emission/opacity significant



R. Sault  
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## Instrumental Challenges

1. **Surface accuracy:** If  $\sigma$  is r.m.s. surface error in  $\mu\text{m}$ , surface efficiency given by Ruze formula:

$$\eta_{\text{sf}} = \exp[-(4\pi\sigma/\lambda)^2]$$

For  $\lambda=3\text{mm}$  and  $\sigma=200\ \mu\text{m}$ ,  $\eta_{\text{sf}}=0.54$ . Antenna “holography” can be used to diagnose large-scale errors in dish shape.

2. **Field of view** (primary beam size):

$$\theta_{\text{FWHM}} \approx \lambda/D \approx 620''/D[\text{m}] \text{ at } 3\text{mm}$$

BIMA:  $D=6.1\text{m}$ ,  $\theta_{\text{FWHM}} = 100''$

ATCA:  $D=22\text{m}$ ,  $\theta_{\text{FWHM}} = 30''$

For large sources, **mosaicing** required.

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## Instrumental Challenges

3. **Pointing accuracy:** For mosaicing, want typical pointing error  $\Delta\theta < \theta_{\text{FWHM}}/20$  (14% amplitude error at half power point). Thus need  $\sim 1.5''$  pointing accuracy at ATCA!

4. **Correlator bandwidth:**

$$1\ \text{MHz} \approx \lambda_{\text{mm}}\ \text{km s}^{-1}$$

The same bandwidth covers only 1.4% of the velocity range at 3mm that it does at 21cm!

5. **Electronic phase noise:** tends to increase with frequency, and hard to calibrate (not antenna-based). For VLA at 22 GHz,  $\phi_{\text{rms}} \sim 10^\circ$ .

6. **Baseline errors:** for a source-cal separation of  $10^\circ$ ,  $\Delta b \sim 0.5\text{mm}$  leads to  $\Delta\phi \sim 10^\circ$ .

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## Amplitude Calibration

Recall that power is often given in temperature units (K) via the conversion:

$$P = k_B T \Delta\nu$$

Calibration of the visibility amplitude is typically performed by comparing it with the **system temperature**, the equivalent noise temperature presented to the detector:

$$T_{\text{sys}} = T_{\text{rec}} + T_{\text{sky}} + T_{\text{dish}} + T_{\text{atc}}$$

The sky temperature can be determined via the radiative transfer equation:

$$T_{\text{sys}} = T_{\text{rec}} + T_{\text{atm}}(1 - e^{-\tau})$$

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## Amplitude Calibration

In practice, we must correct  $T_{\text{sys}}$  for atmospheric absorption in order to estimate what the **unattenuated** celestial signal would be:

$$T_{\text{sys,eff}} = T_{\text{sys}} e^{\tau} = e^{\tau} [T_{\text{rec}} + T_{\text{atm}}(1 - e^{-\tau})]$$

Example for  $T_{\text{rec}}=150$  K,  $T_{\text{atm}}=290$  K:

|                      |     |     |      |
|----------------------|-----|-----|------|
| $\tau$               | 0.2 | 0.8 | 2.0  |
| $T_{\text{sys}}$     | 200 | 310 | 400  |
| $T_{\text{sys,eff}}$ | 250 | 690 | 2960 |

The opacity  $\tau$  at a given frequency depends on the column of precipitable water vapour (PWV).

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## Chopper Wheel Method

The standard method for measuring  $T_{\text{sys,eff}}$  involves measuring the power received from the blank sky, then placing an ambient (295 K) load in front of the receiver (Kutner & Ulich 1981).

In both cases the output power is given by

$$P_{\text{out}} = m (T_{\text{inp}} e^{-\tau} + T_{\text{sys}}) = m e^{-\tau} (T_{\text{inp}} + T_{\text{sys,eff}})$$

where  $m$  is some scale factor and  $T_{\text{inp}}$  is the temperature of a "load" **above the atmosphere**.

For the blank sky measurement,  $T_{\text{inp}} = T_{\text{CMB}} = 3$  K.

For the ambient load measurement,  $T_{\text{inp}} = T_{\text{amb}} = 295$  K. (although the load isn't above the atmosphere, if the atmosphere is also at 295 K, its absorption and emission would cancel anyway)

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## Chopper Wheel Method

Combining the two measurements yields:

$$\frac{P_{\text{amb}}}{P_{\text{sky}}} = \frac{T_{\text{amb}} + T_{\text{sys,eff}}}{T_{\text{cmb}} + T_{\text{sys,eff}}}$$

$$T_{\text{sys,eff}} = \frac{(T_{\text{amb}} - T_{\text{cmb}})P_{\text{sky}}}{P_{\text{amb}} - P_{\text{sky}}} - T_{\text{cmb}} \approx \frac{(290\text{K})P_{\text{sky}}}{P_{\text{amb}} - P_{\text{sky}}}$$

Hence, subject to the approximation  $T_{\text{amb}} \approx T_{\text{atm}}$ , the chopper wheel method gives  $T_{\text{sys,eff}}$  directly even when  $T_{\text{sys}}$  and  $\tau$  are not separately known!

**Regular systemp measurements (every 15 min. or so) are needed to track variations in the receiver gains and atmosphere.**

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## Absolute Flux Calibration

Good flux calcs are unresolved, bright, and non-varying. But no such objects at mm wavelengths!

For planets there are reasonably good models for  $T_b$  which can be used, together with angular size, to derive a visibility model.

$$S_v = \frac{2kT_b}{\lambda^2} \Omega_{disk}$$

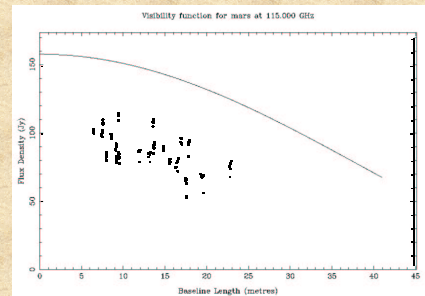
where  $\Omega_{disk}$  is the angular size of the planet.

Usual method:

- Observe a planet during your track for 5-10 min.
- Bootstrap fluxes of phase calibrator & source using a model for the planet visibility structure.

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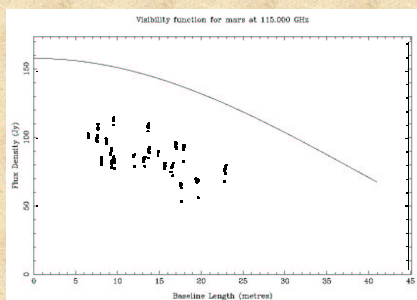
## Absolute Flux Calibration



Problem: planets will generally be resolved out by the interferometer.

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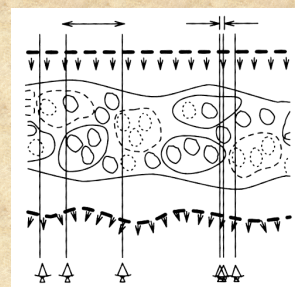
## Absolute Flux Calibration



Possible solution: bootstrap in single-dish rather than interferometer mode.

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## Atmospheric Phase Noise

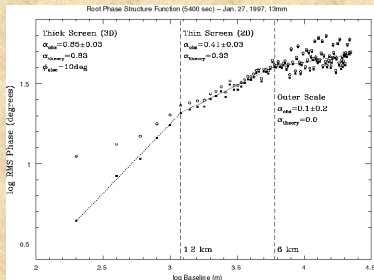


Changes in refractive index of atmosphere due to precipitable water vapor (PWV) lead to "corrugations" in wavefront of an incoming plane wave.

Desai 1998

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## Atmospheric Phase Noise

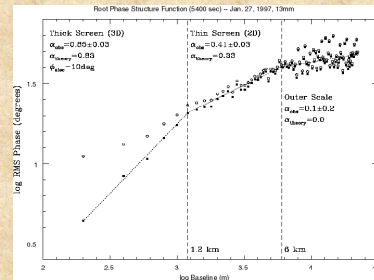


Carilli et al., 1999

- Atmospheric RMS phase noise ( $\phi_{rms}$ ) increases with **baseline length** because turbulence occurs on a range of length scales.

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## Atmospheric Phase Noise



Carilli et al., 1999

- Phase noise also increases with **frequency** because refractive effects are largely non-dispersive (constant in length units).

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## Effect on Visibility Data

Effect of phase noise on a visibility measurement can be expressed as

$$\langle V \rangle / V_0 = \exp(-\phi_{rms}^2 / 2)$$

where  $\phi_{rms}$  is the RMS phase variation during the averaging time.

For  $\phi_{rms}=1$  rad,  $\langle V \rangle / V_0 = 0.60$  and the visibility amplitude is reduced by 40% due to phase noise (also called **decorrelation**).

Since  $\phi_{rms}$  increases with baseline length, visibility amplitude falls off in the outer (**u,v**) plane, degrading the angular resolution of the map (equivalent to optical "seeing").

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## Phase Calibration

- Standard technique (**phase referencing**): observe a point source as phase calibrator every  $t_c \sim 20$ -30 minutes, then apply interpolated phase gains to source.
- Can measure phase variations over timescales  $> 2t_c$  (Nyquist).
- OK for baselines up to  $\sim 100$  m (looking through similar stuff) but time-averaged phase fluctuations too large on longer baselines.
- ATCA baselines range from 30m to 3km – **alternative techniques required**.

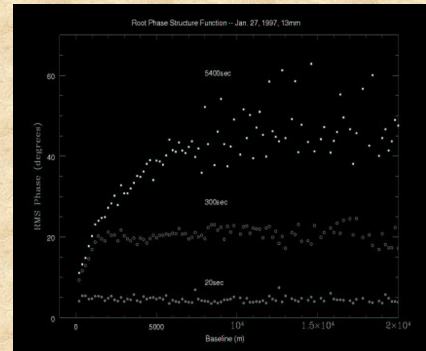
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## Phase Calibration

1. If source structure is simple and  $n_{\text{bsln}} > 3$ , can correct phase on much shorter timescales via **self-calibration** (limited by S/N ratio).
2. Otherwise, must switch back to phase calibrator rapidly (every few minutes) – **fast switching**.
3. With extra antennas, can observe calibrator continuously using a subarray – **paired array**.
4. Can make precise measurements of the water vapor column (PWV), proportional to the phase delay, by measuring  $\text{H}_2\text{O}$  lines at 22 or 183 GHz – **water vapor radiometry** (see Bob Sault's talk).
  - In the near term, fast switching will be the preferred method for ATCA.

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## Effectiveness of fast switching



Carilli et al. 1999

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## Observing a test calibrator

In poor weather or when using long baselines, it may be unclear whether a non-detection is due to source weakness or to atmospheric phase decorrelation.

**Procedure:** observe a weaker (but detectable) “test” quasar near your source, in addition to a stronger quasar as the phase calibrator.

If phase gains transferred to the test quasar yield a good detection, your phase calibration is probably adequate.

**Example:** observe test quasar instead of source every third cycle (30 sec/cycle).

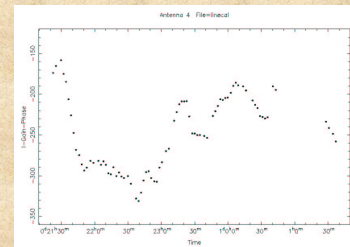
```
source=m82,0841+708,1048+717
```

```
grid='ns(1,1,1,2,2,1,1,1,2,2,3,3,3,2,2)'
```

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## Instrumental Phase

- Phase variations can also result from variable instrumental delays, e.g. diurnal changes in effective cable length.
- A roundtrip phase measurement can be used to correct for these delays.

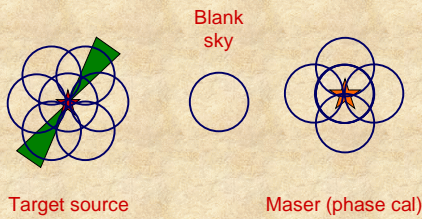


Four hours at BIMA

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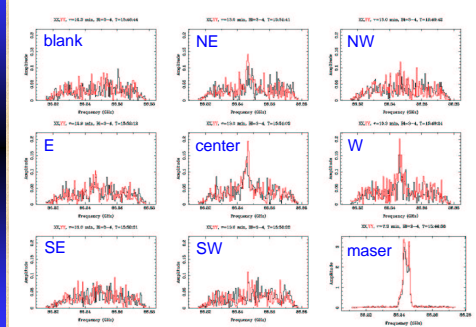
## Sample Observing Scheme

1. Pointing pattern on SiO maser
2. 9-pt mosaic, 30 sec/point, repeated for 45 min.
3. Blank sky position serves as OFF for AC data



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## Results for NGC 6334 I(N)



Single-baseline ATCA, July 2001

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## Lecture Summary

- Interferometry at high radio frequencies places stringent demands on **pointing, surface accuracy**, and other instrumental properties.
- Amplitude calibration is complicated by varying **atmospheric opacity**, but can be corrected to first order using the chopper wheel method.
- Flux calibration relies on **planets** because quasars are variable at mm wavelengths.
- Phase calibration becomes increasingly difficult at **higher frequencies** and **longer baselines** due to turbulence in the tropospheric H<sub>2</sub>O layer.
- **Observing programs need to allot adequate time for amplitude, flux, phase, and pointing calibrations in order to minimise map errors.**

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