

The Signal Path

John Reynolds



Picture © Paul Varley

The “Dish” Advantage

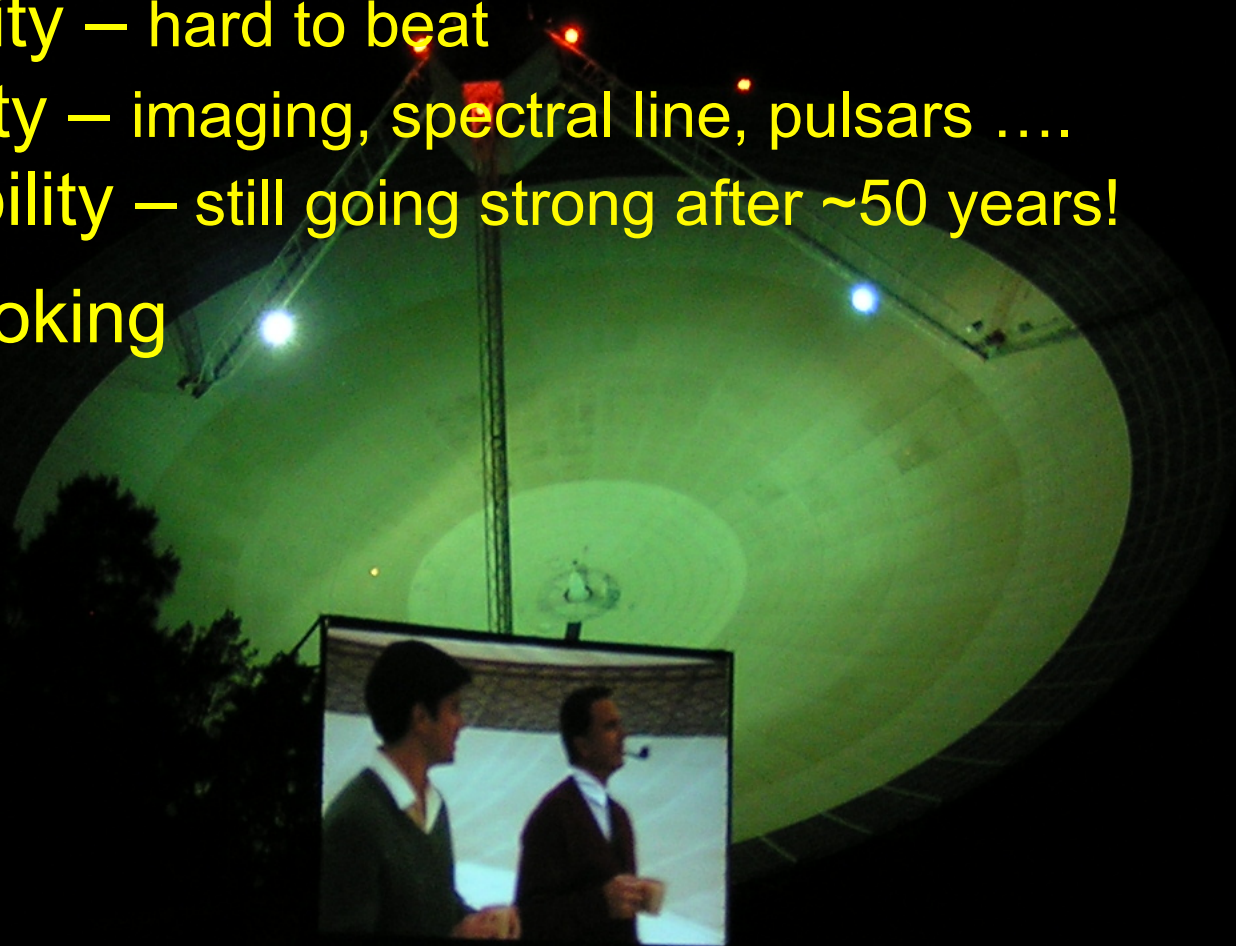
Simplicity – cost effective for collecting area

Sensitivity – hard to beat

Versatility – imaging, spectral line, pulsars

Adaptability – still going strong after ~50 years!

Good looking



And not done yet



© INAF:- Osservatorio Astronomico di Cagliari

Overview

- Signal Path: the basics
 - Conversion systems
 - Sampling theorem (re)visited
 - Samplers (aka digitizers, ADCs)
- Calibration
 - Noise cal injection
 - Single-dish strategies

How complicated can it be?

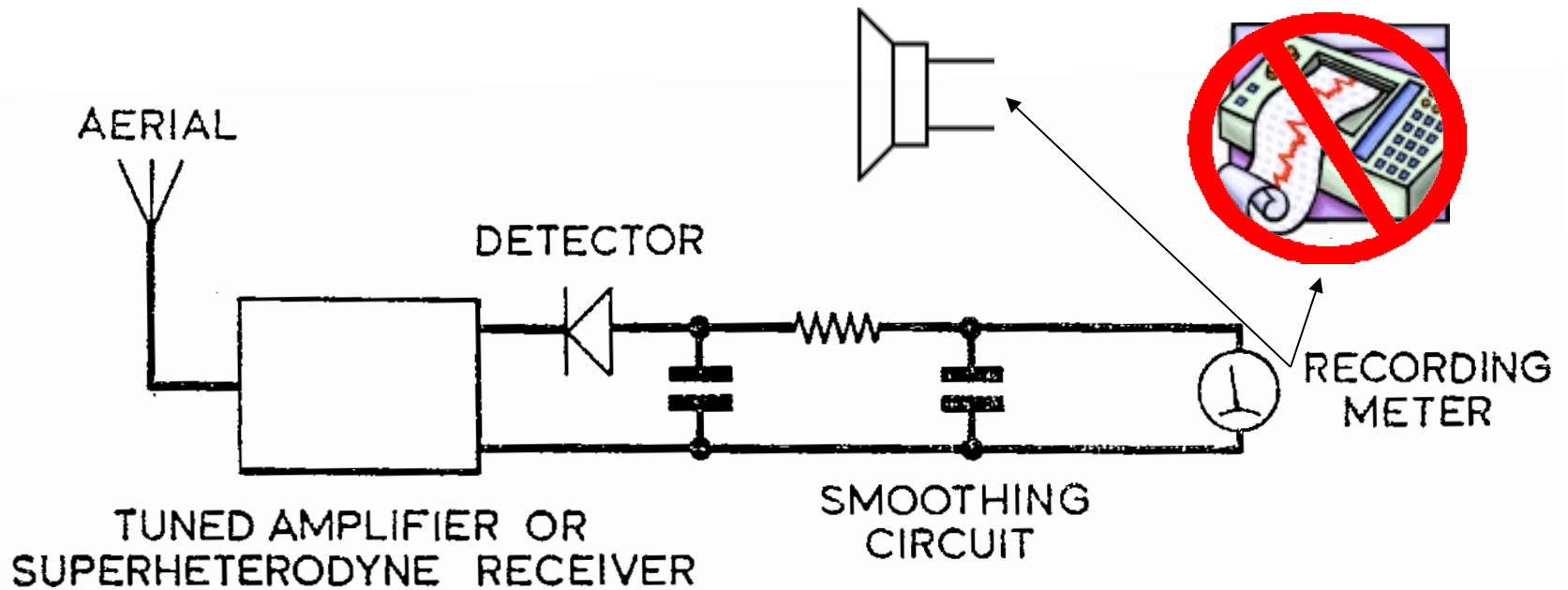
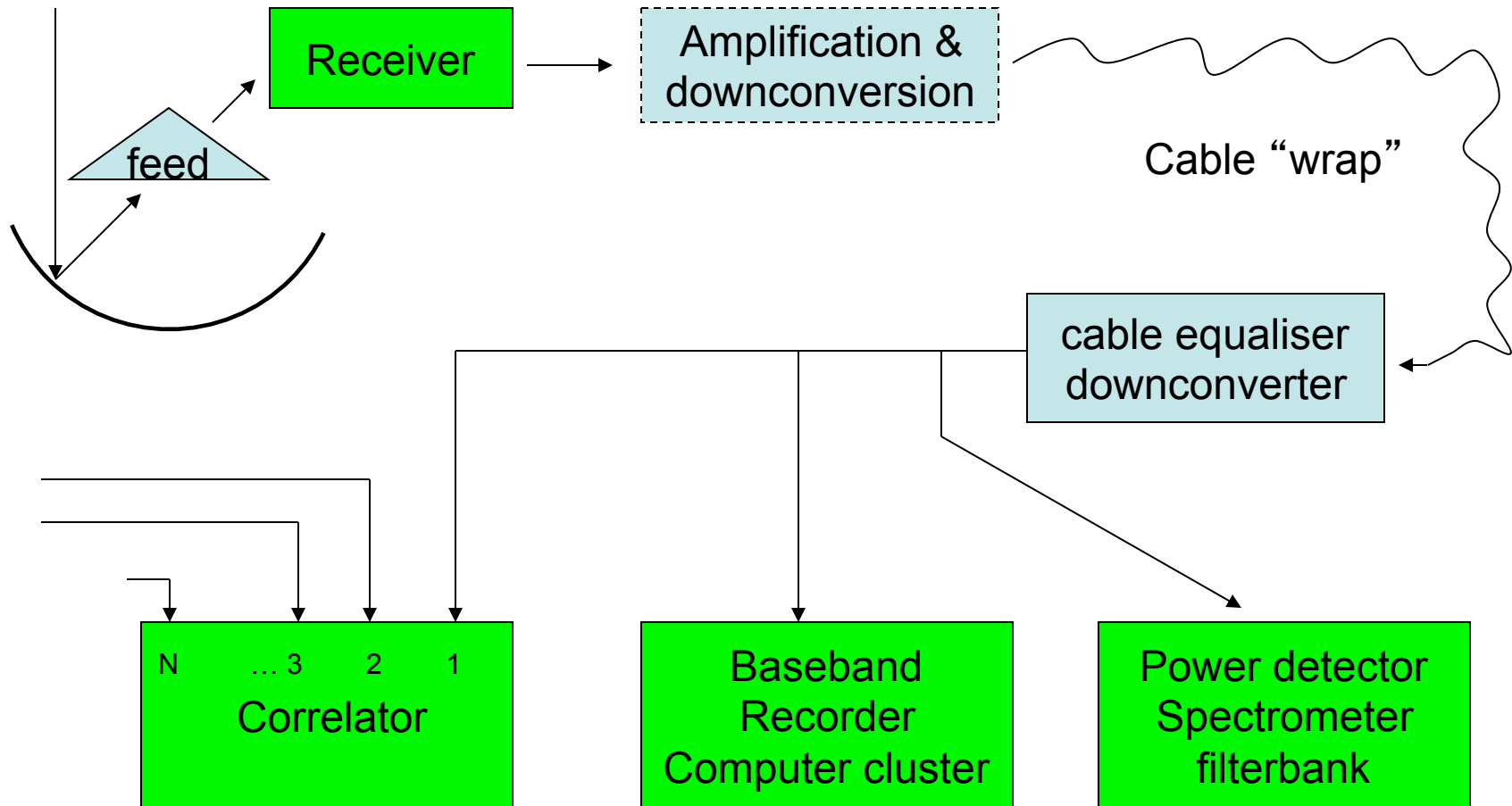


Fig. 2. A simple radio astronomy receiver

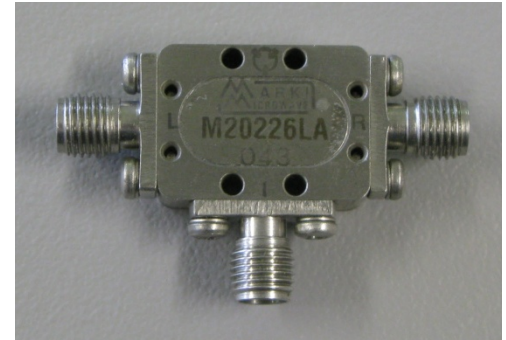
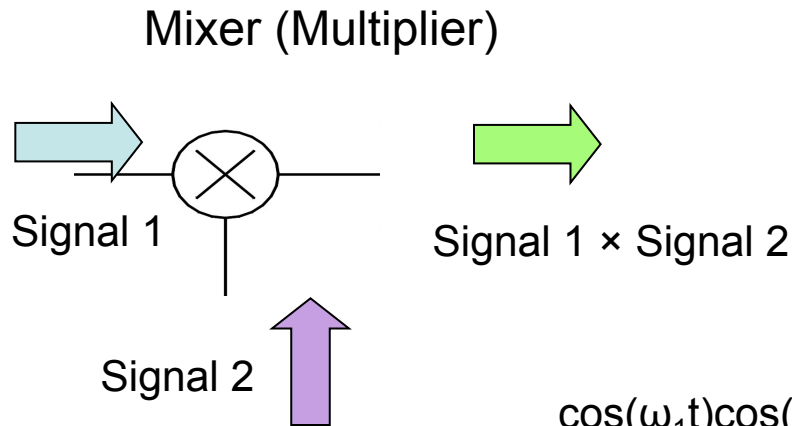
From "Radio Astronomy", R.C.Jennison (1966)



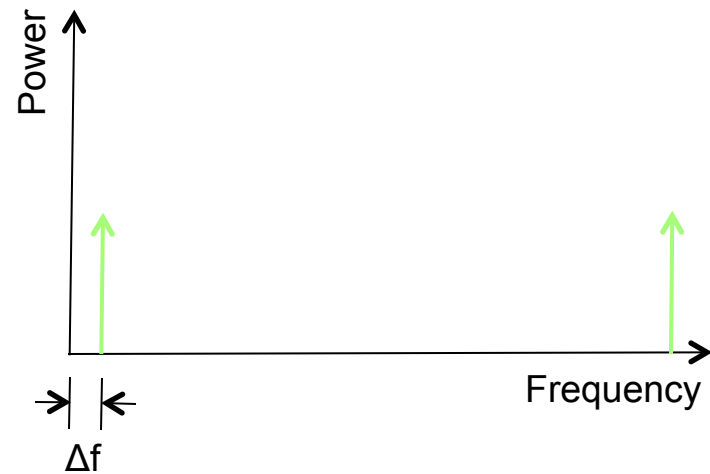
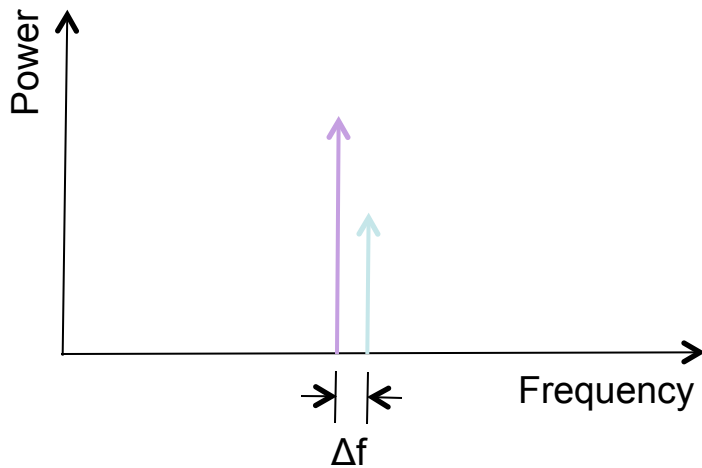
Signal path – the basics



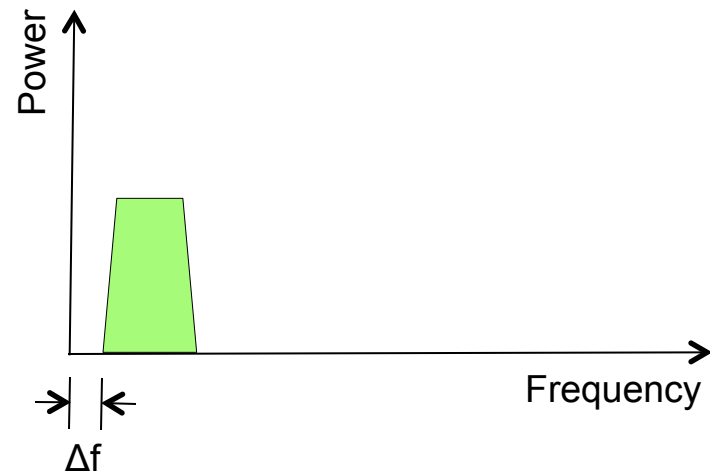
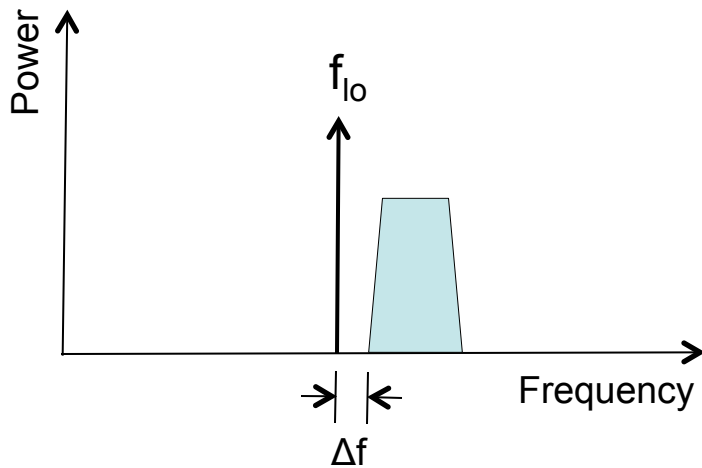
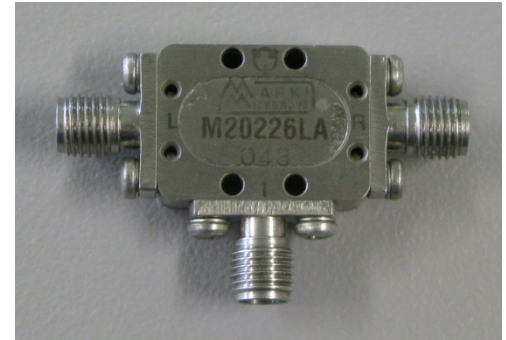
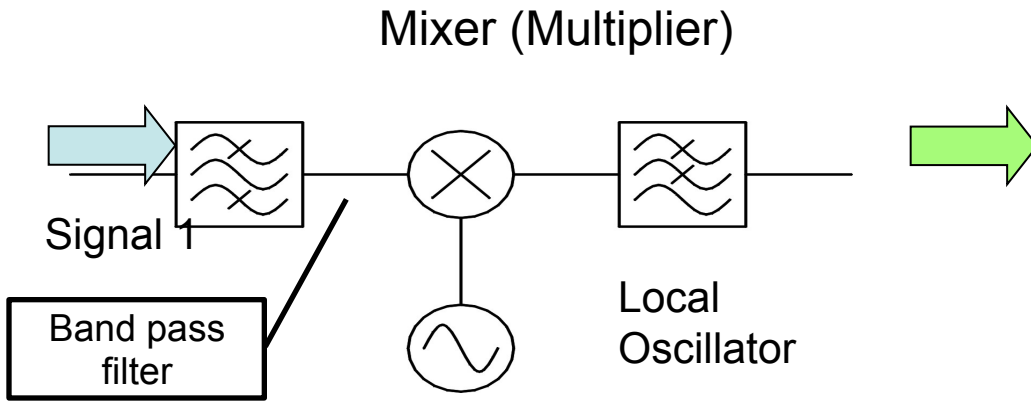
Mixing it down – Frequency Conversion



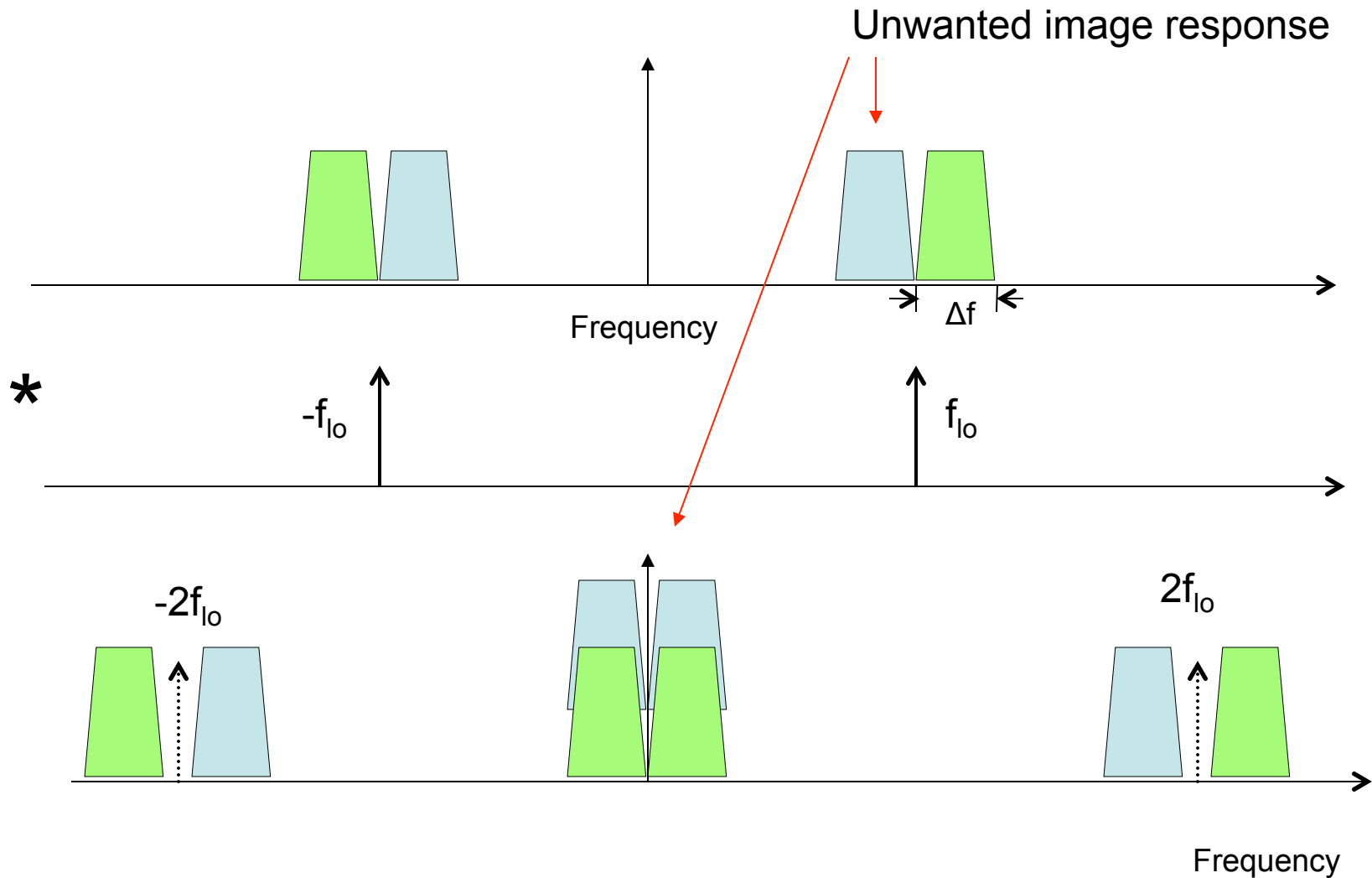
$$\cos(\omega_1 t)\cos(\omega_2 t) = \frac{1}{2}[\cos((\omega_1 + \omega_2)t) + \cos((\omega_1 - \omega_2)t)]$$



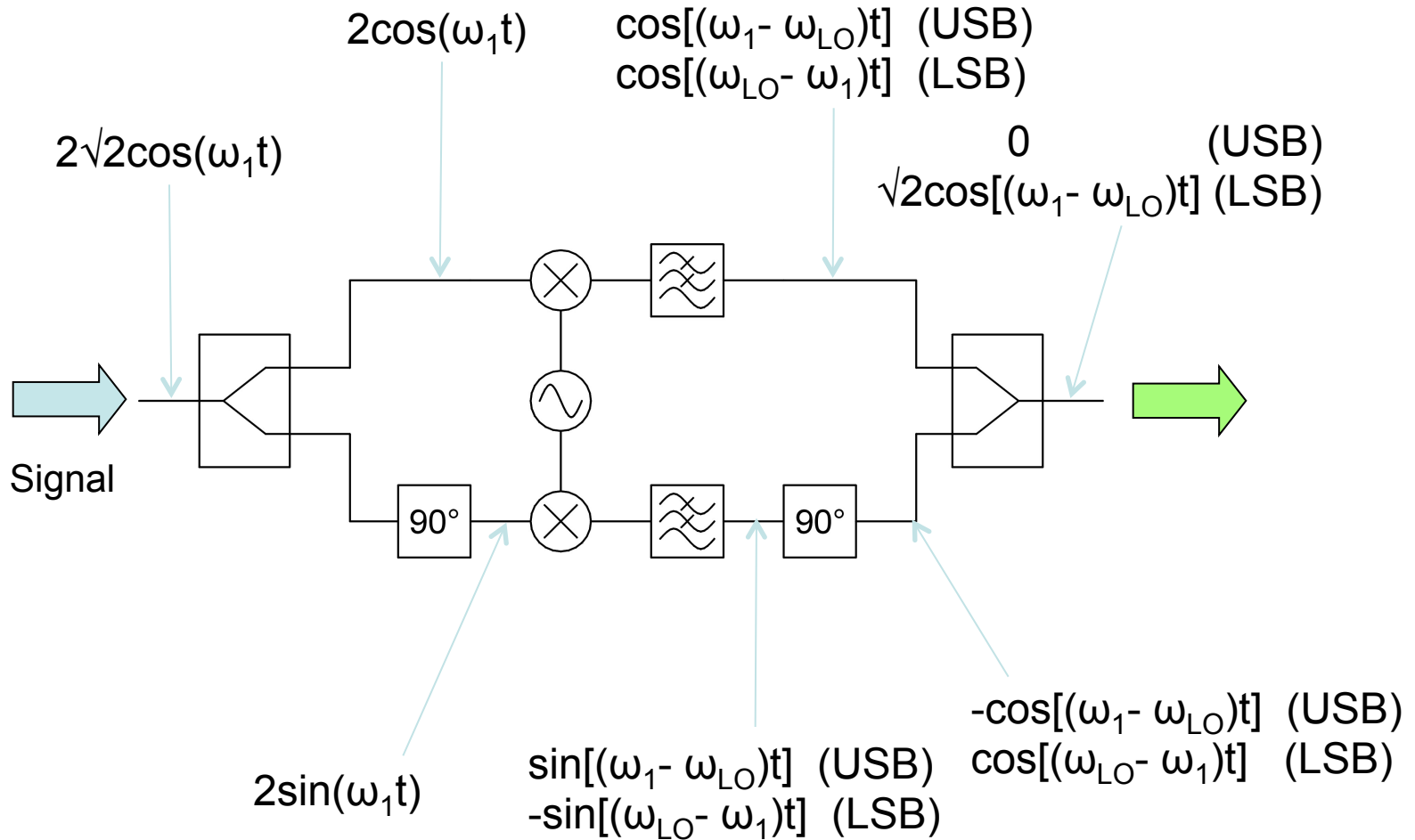
Mixing it down II– Frequency Conversion (aka superheterodyne principle)



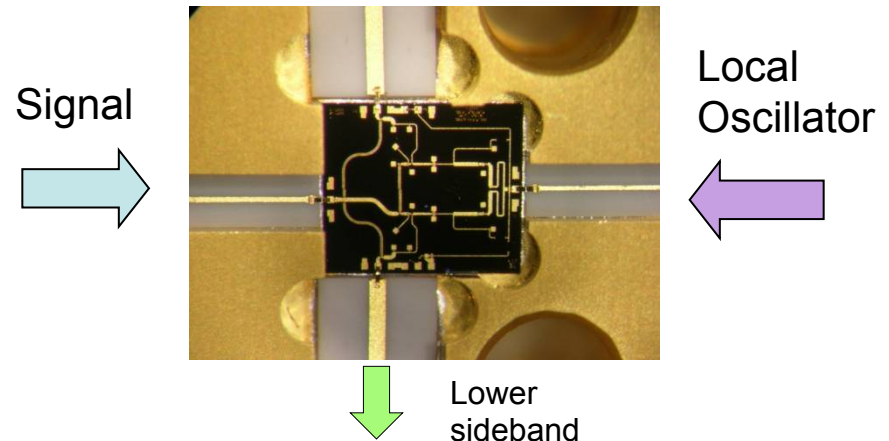
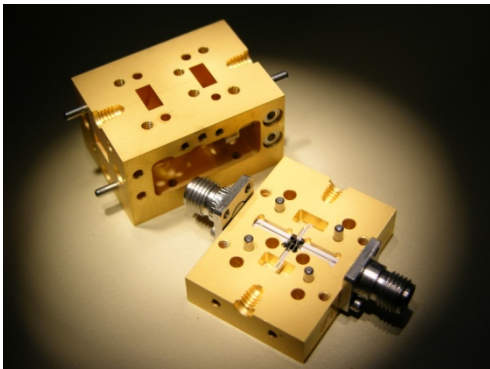
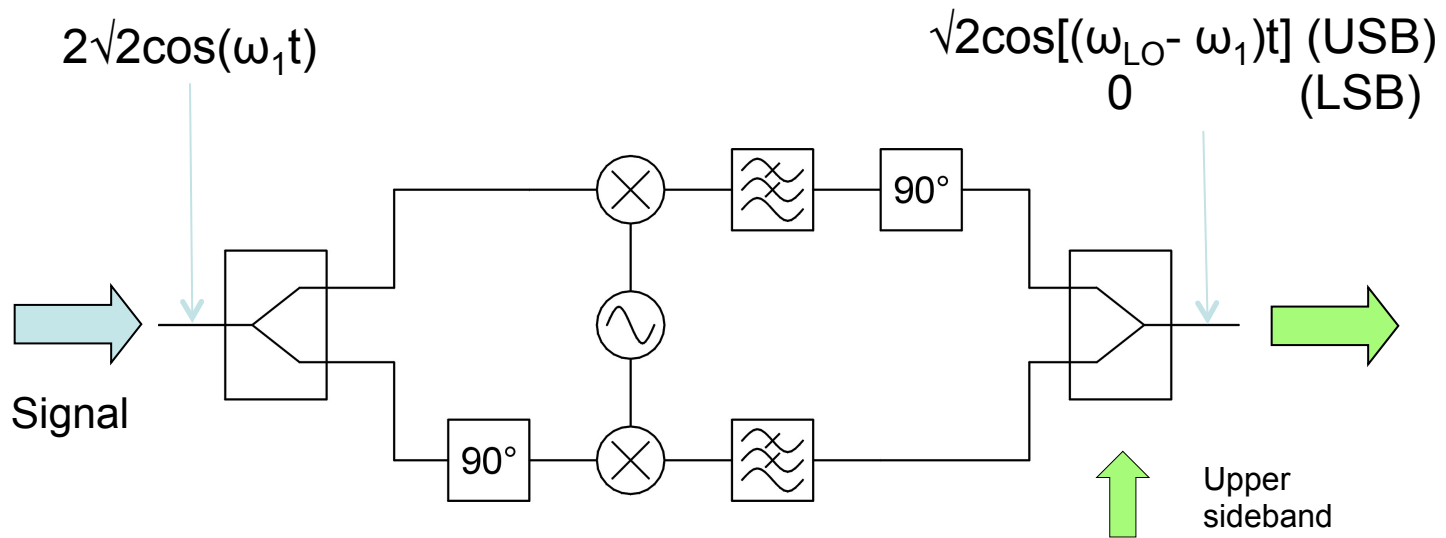
Real-world problems



Single Sideband Mixers



Single Sideband Mixers



Filterbanks,
VS
spectrometers
VS
correlators

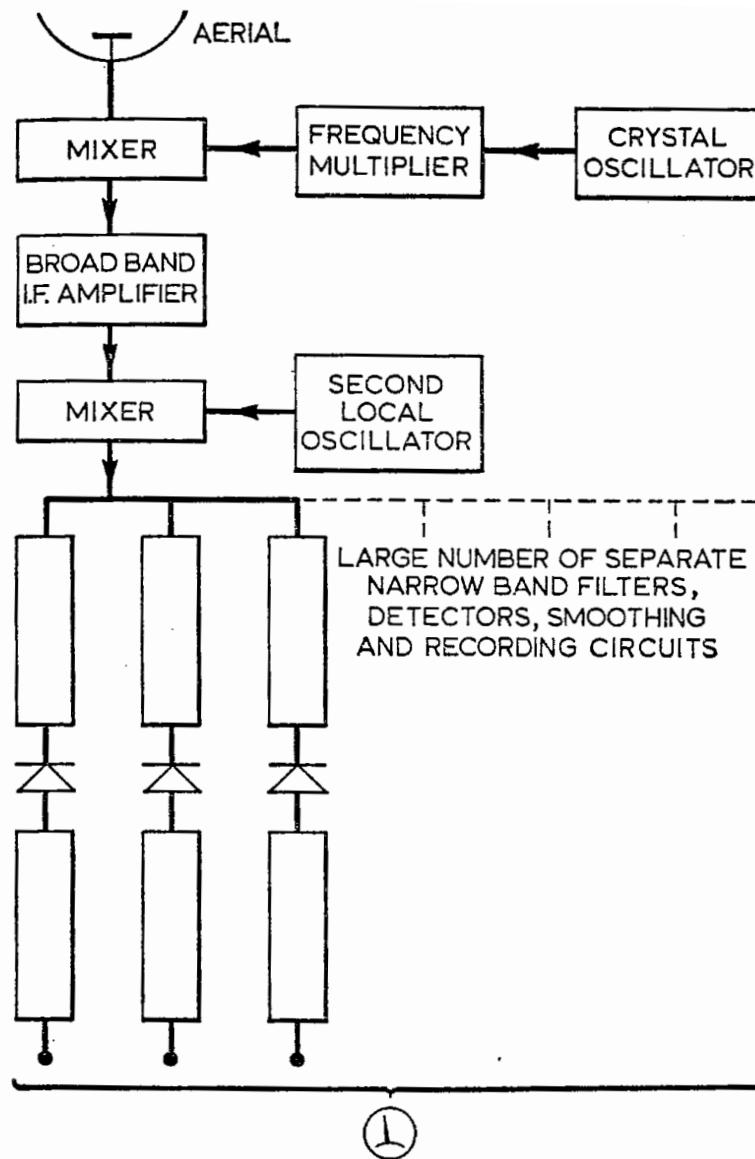
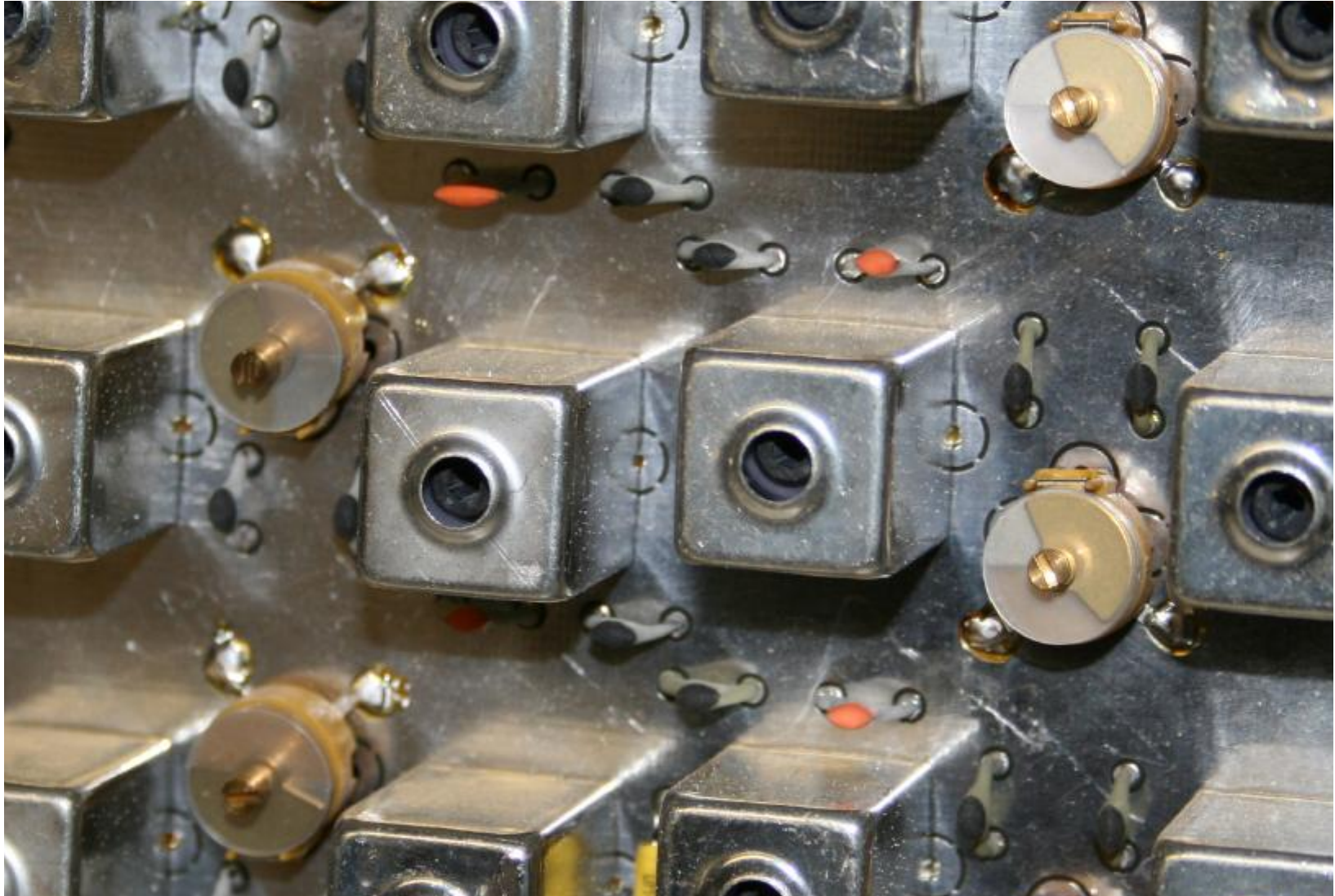


Fig. 7. Simple multi-channel hydrogen line spectrometer receiver

The last great analogue filterbank?



Sampling Theorem – History

The theorem is commonly called the **Nyquist sampling theorem**; since it was also discovered independently by [E. T. Whittaker](#), by [Vladimir Kotelnikov](#), and by others, it is also known as **Nyquist Shannon–Kotelnikov**, **Whittaker–Shannon–Kotelnikov**, **Whittaker–Nyquist–Kotelnikov–Shannon**, **WKS**, etc., sampling theorem, as well as the **Cardinal Theorem of Interpolation Theory**.

It is often referred to simply as *the sampling theorem*.

(From Wikipedia)

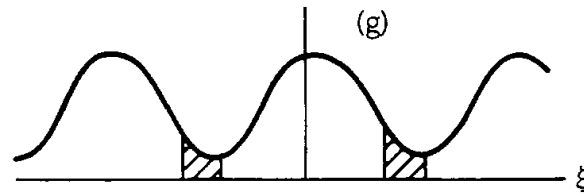
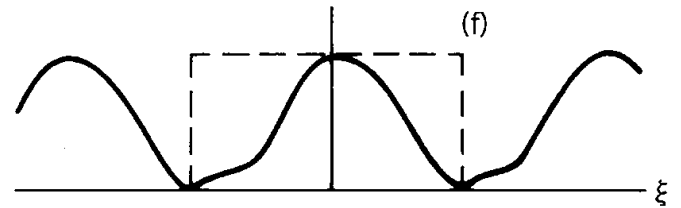
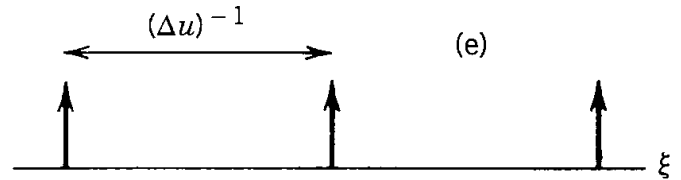
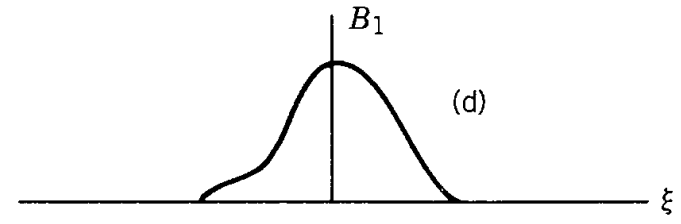
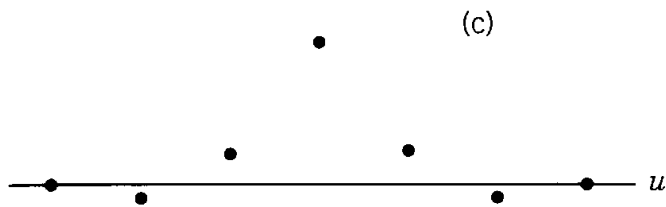
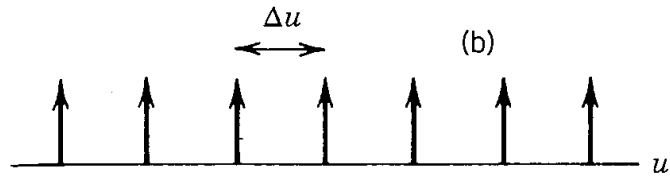
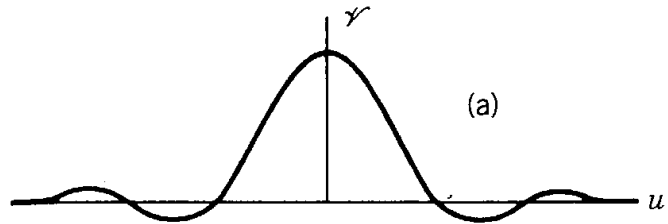
Sampling Theorem (Shannon)

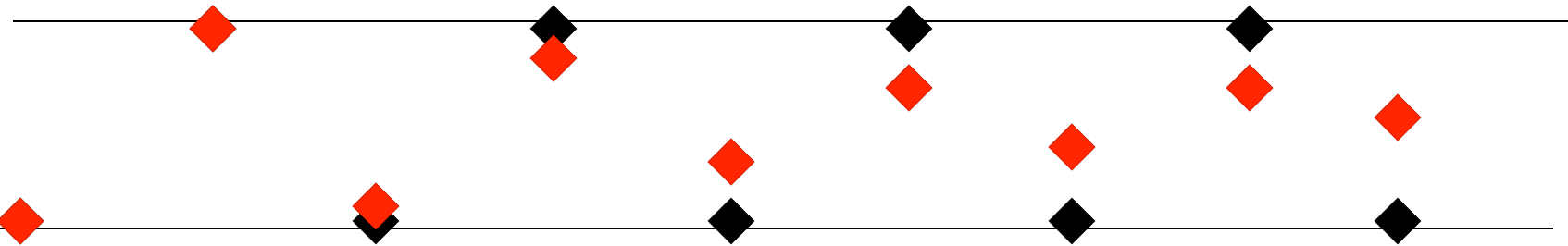
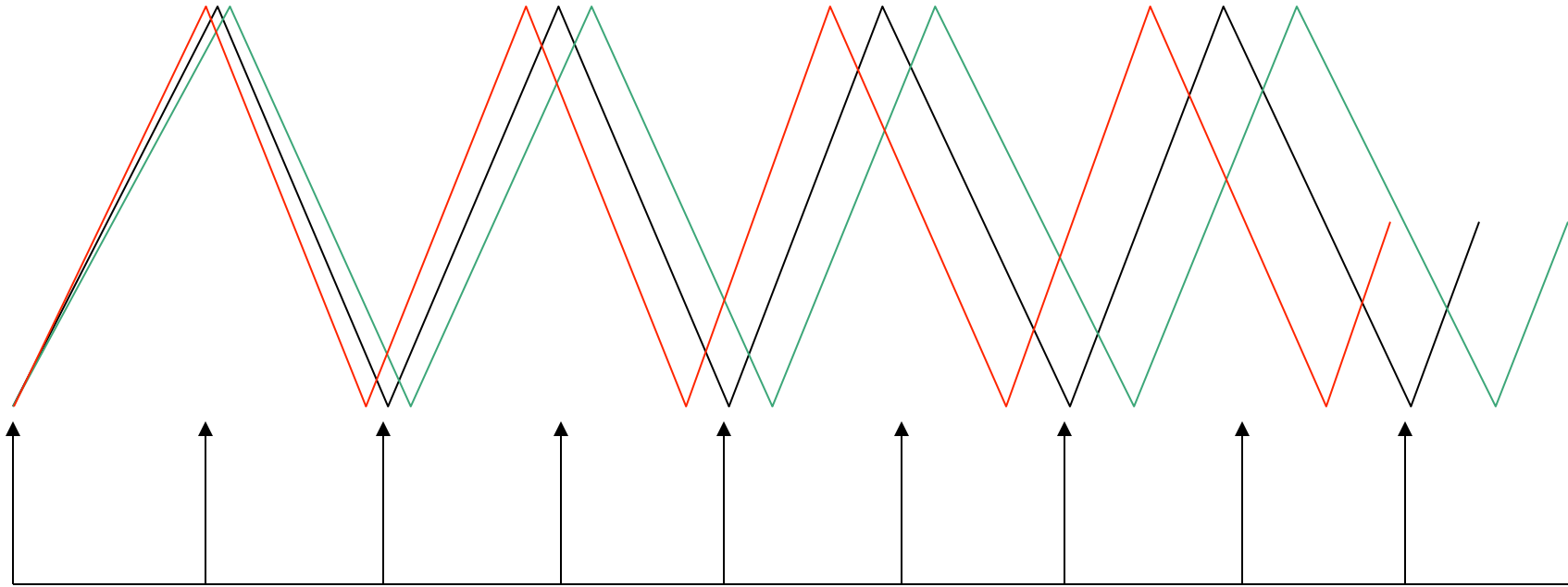
If a function $x(t)$ contains no frequencies higher than B hertz, it is completely determined by giving its ordinates at a series of points spaced $1/(2B)$ seconds apart.

$$t_{\text{samp}} < 1 / 2B$$



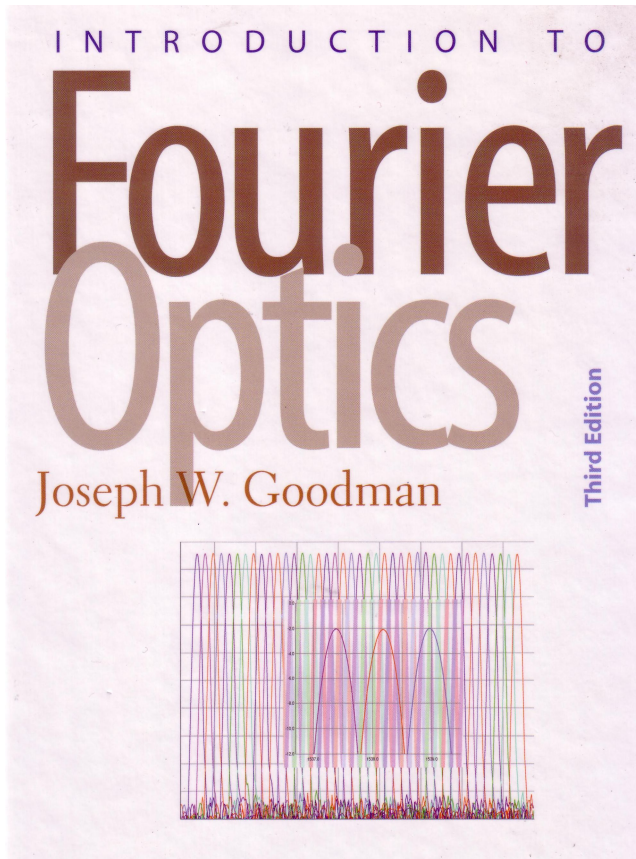
Sampling Theorem





$t_s = 1/BB \times 2$ (Nyquist sampled)

Sampling Theorem continued



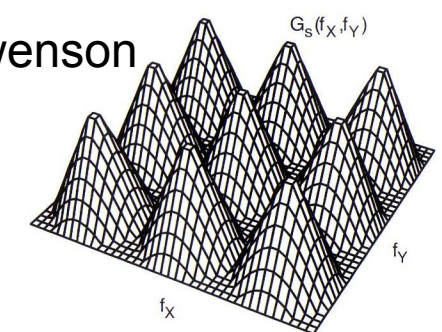
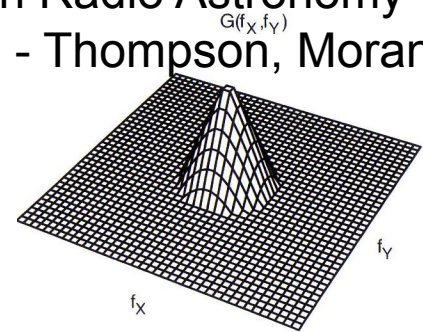
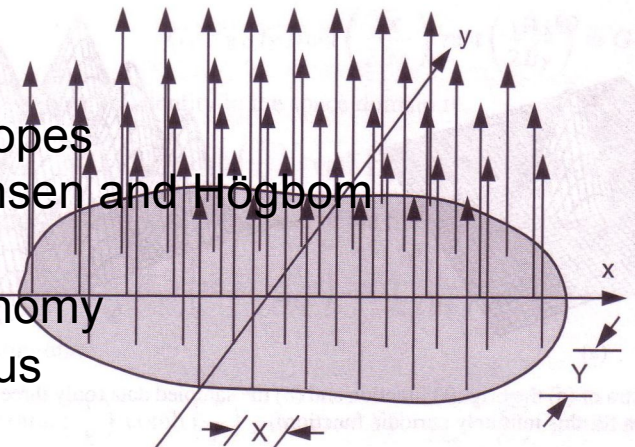
Also;

Radiotelescopes
– Christiansen and Högbom

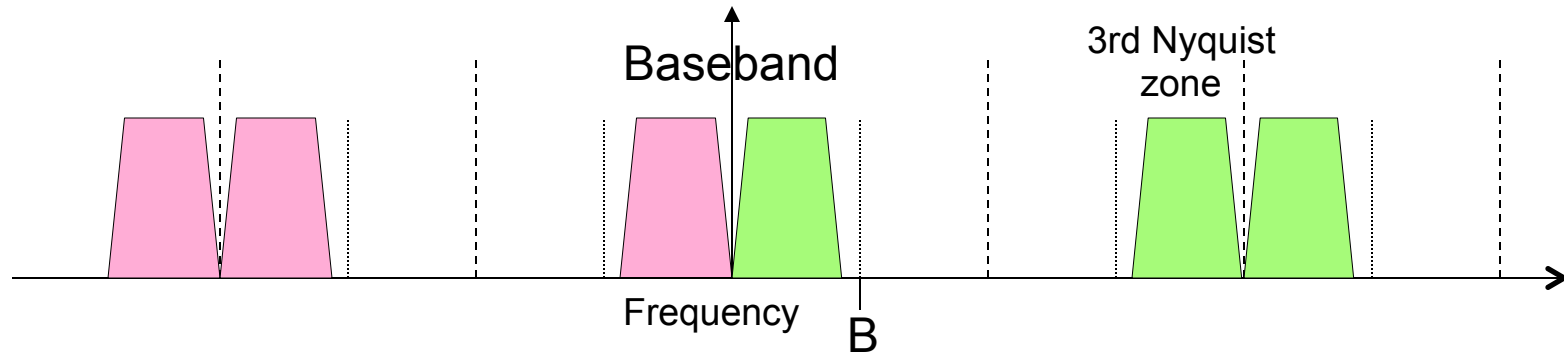
Radio Astronomy
– J.D. Kraus

Principles of Interferometry and Synthesis
in Radio Astronomy

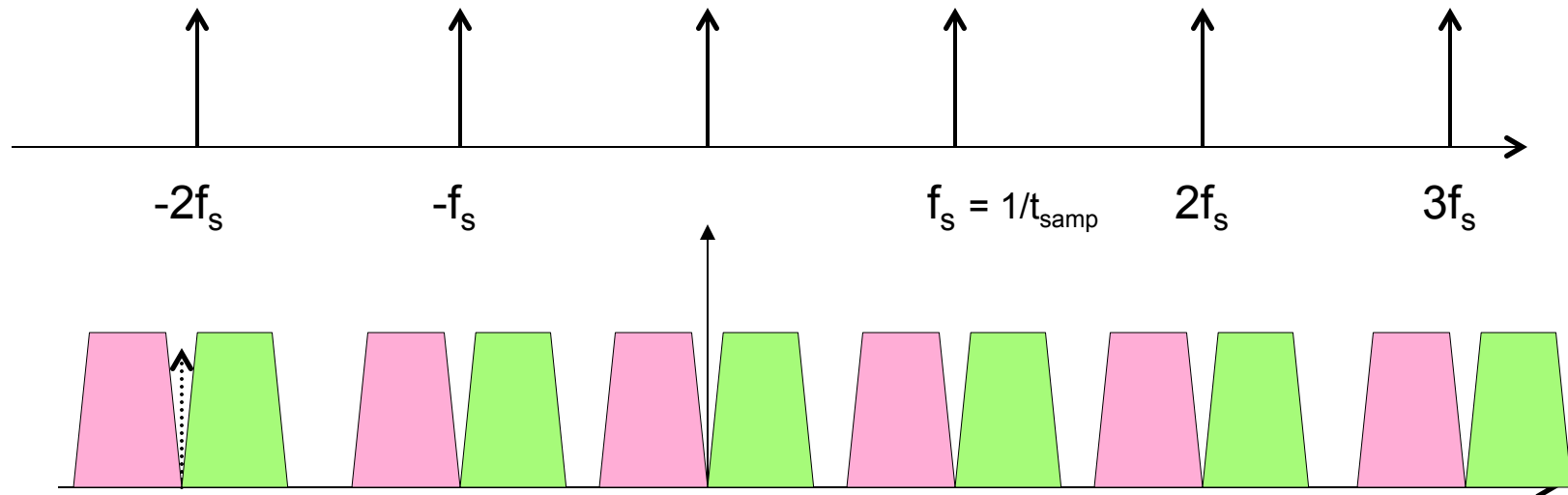
- Thompson, Moran, Swenson



Aliased sampling

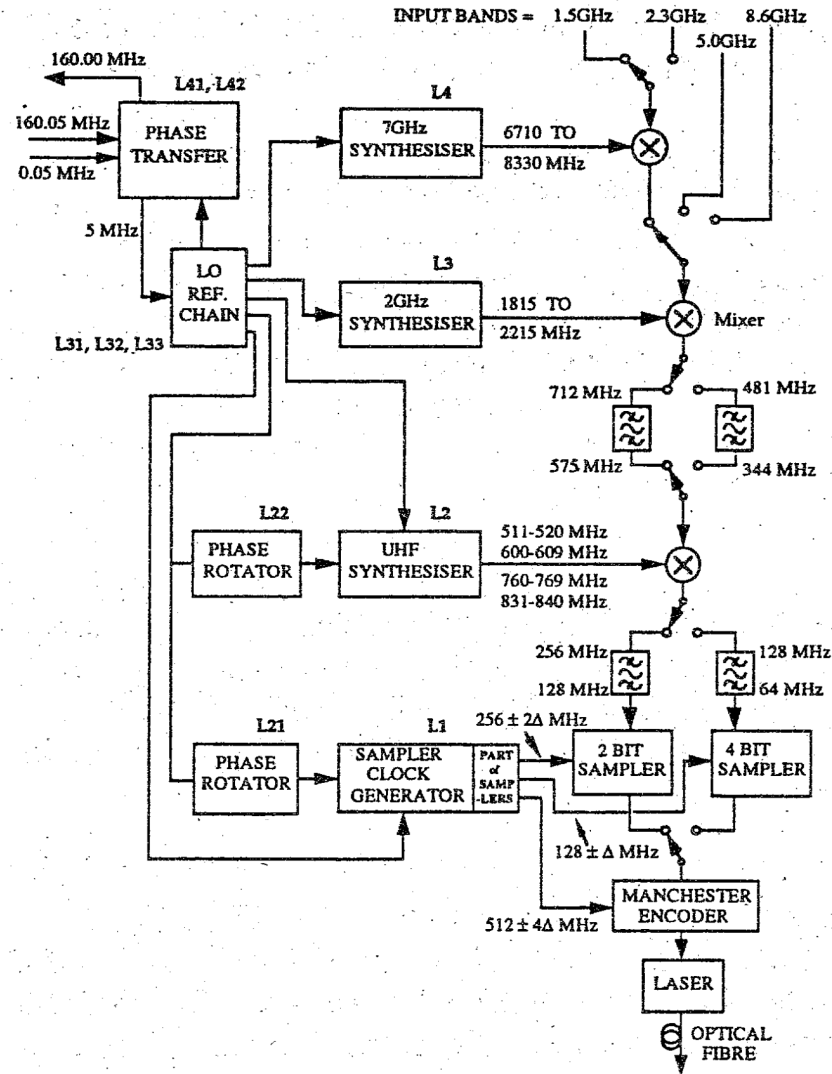


*



Sampling theorem: $f_s = 1/t_{\text{samp}} > 2B$

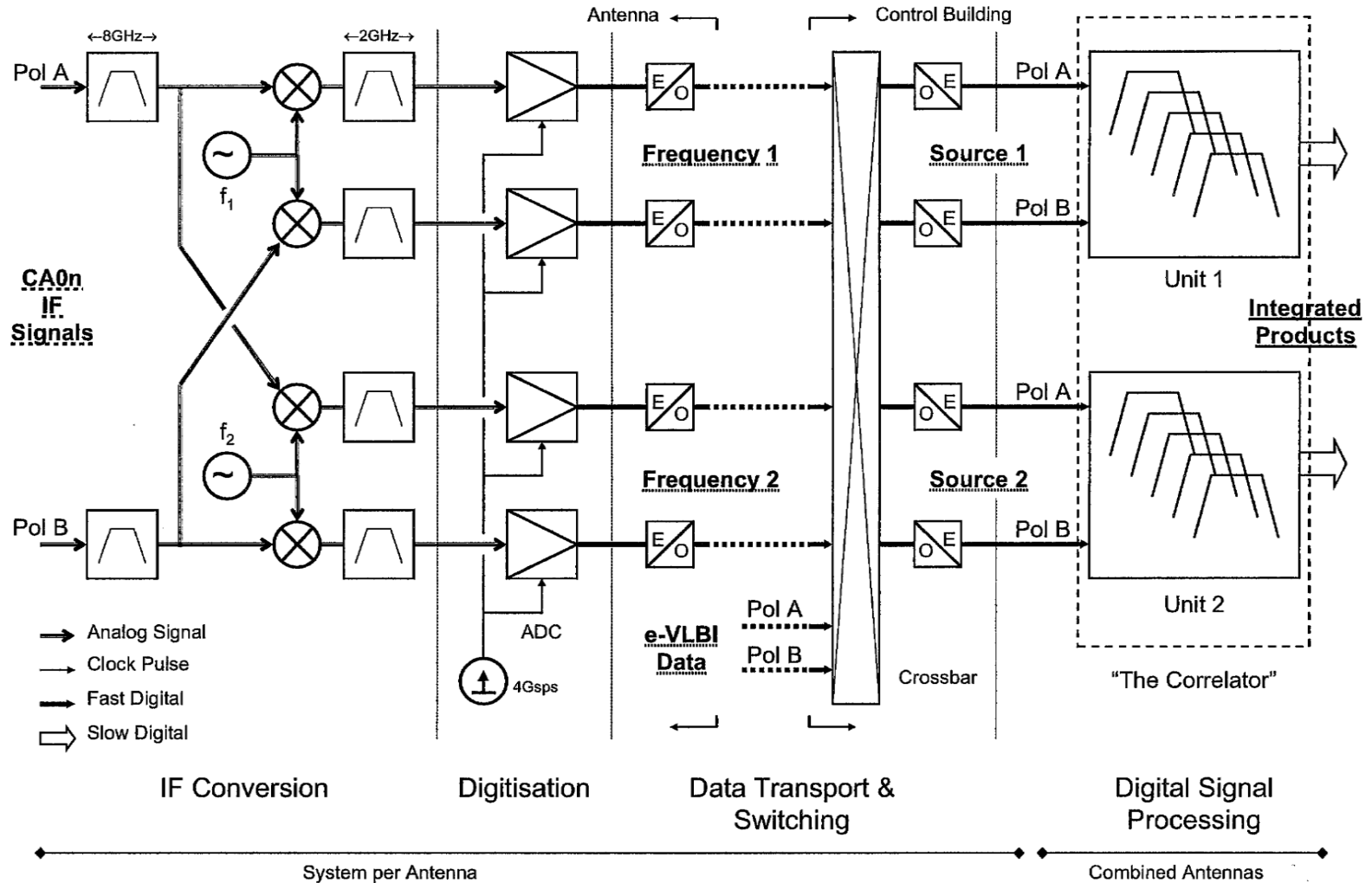
The old ATCA conversion chain



Recent Trends

- Faster, cheaper, samplers
 - Faster, cheaper processing, data storage
- Wider sampled bandwidths
- Fewer downconversion
- “direct conversion” (no downconversion)
e.g. DRAO receiver at Parkes)

CABB signal path



Out of scope

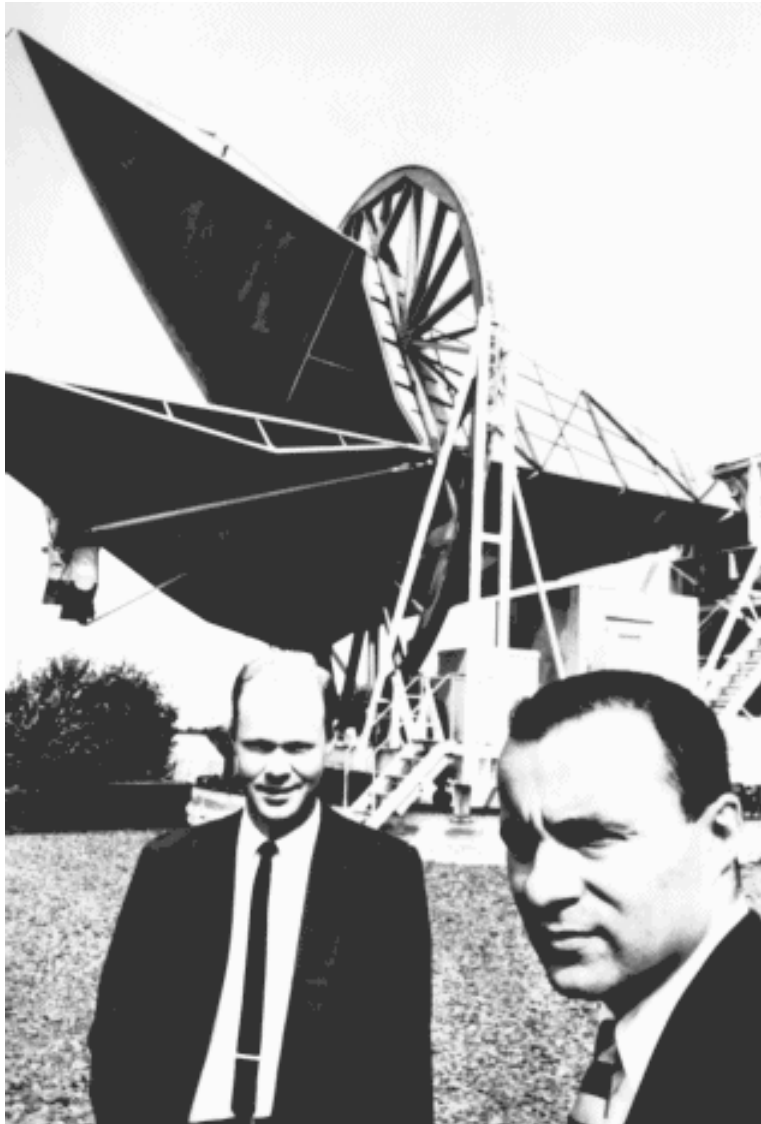
- Limits;
 - Distortion: harmonic, intermodulation
 - Finite precision sampling (1-bit, 2-bit ...)

 - The joys of cabling
 - “RFoF” – RF over fibre

- Complexities
 - Complex sampling

Calibration

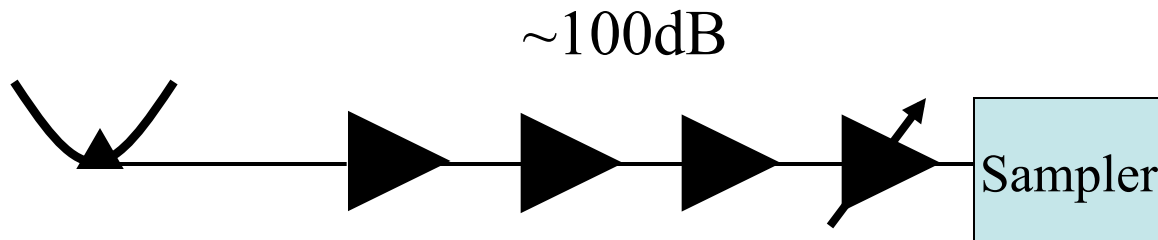
You never know – it might be important.



What are we measuring?

- Typical receiver systems have large gain which varies with time.

Abandon detected power for calibration:
use only equivalent noise temperatures.



Dicke Switch

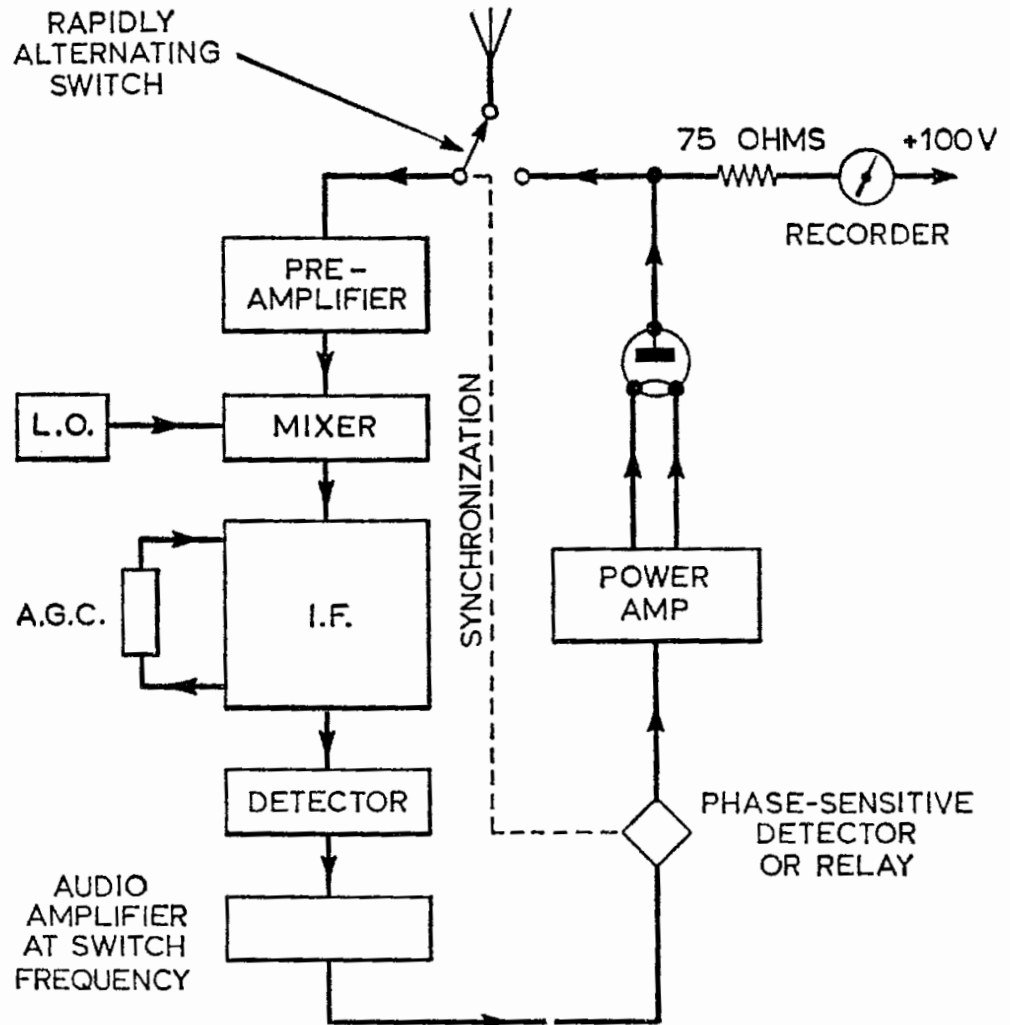
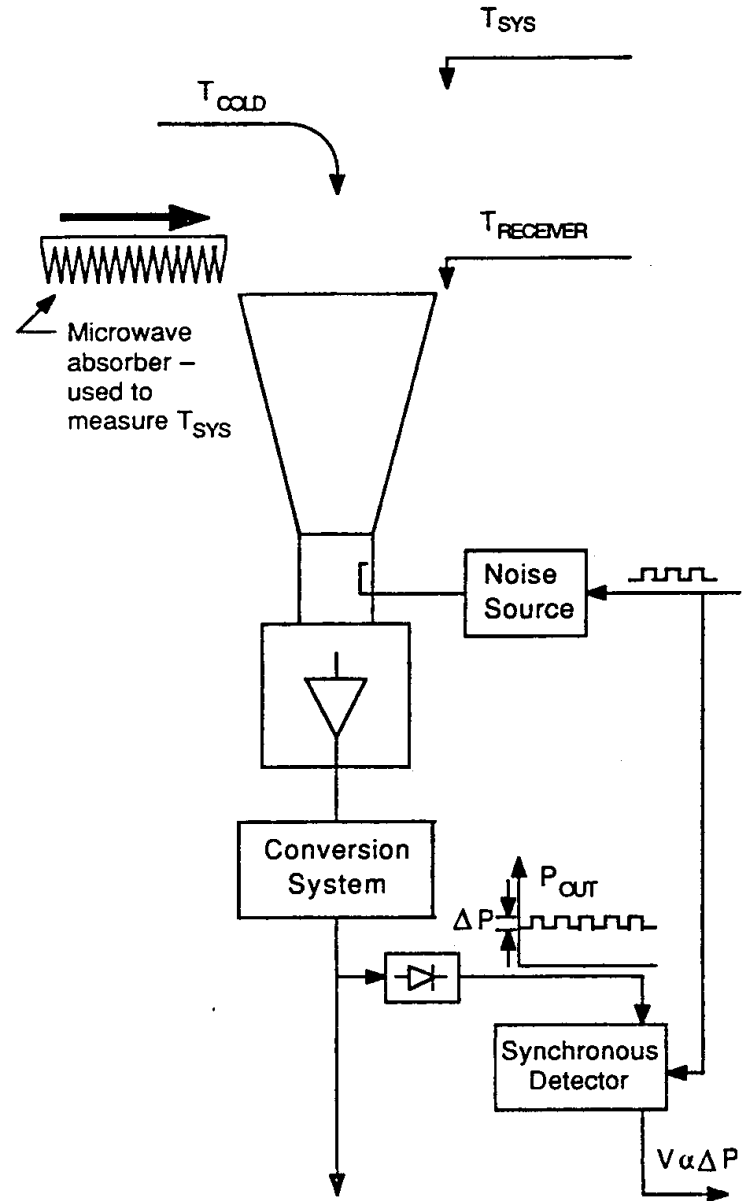


Fig. 3. A servo controlled receiver in which the signal is rapidly compared with that from a noise diode (Ryle and Vonberg, following a principle first used by R. H. Dicke)

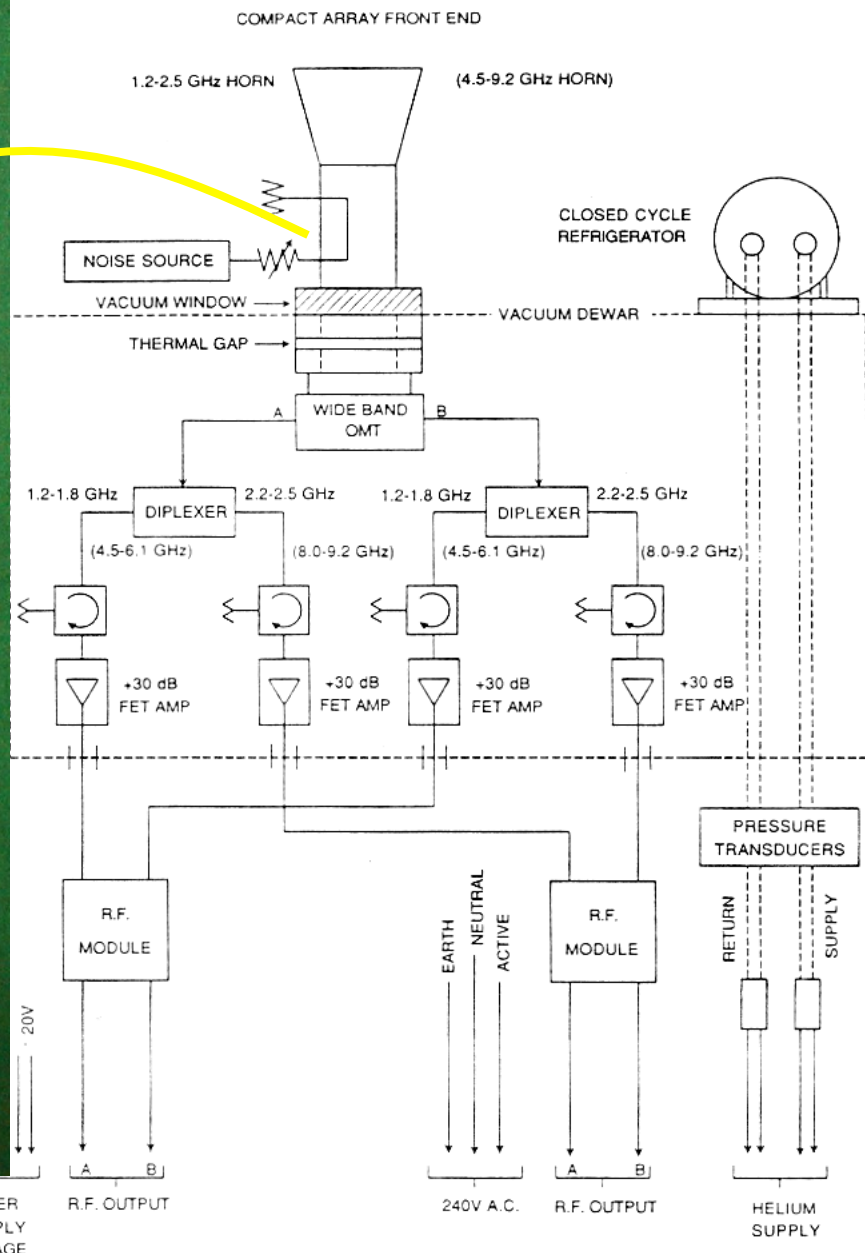
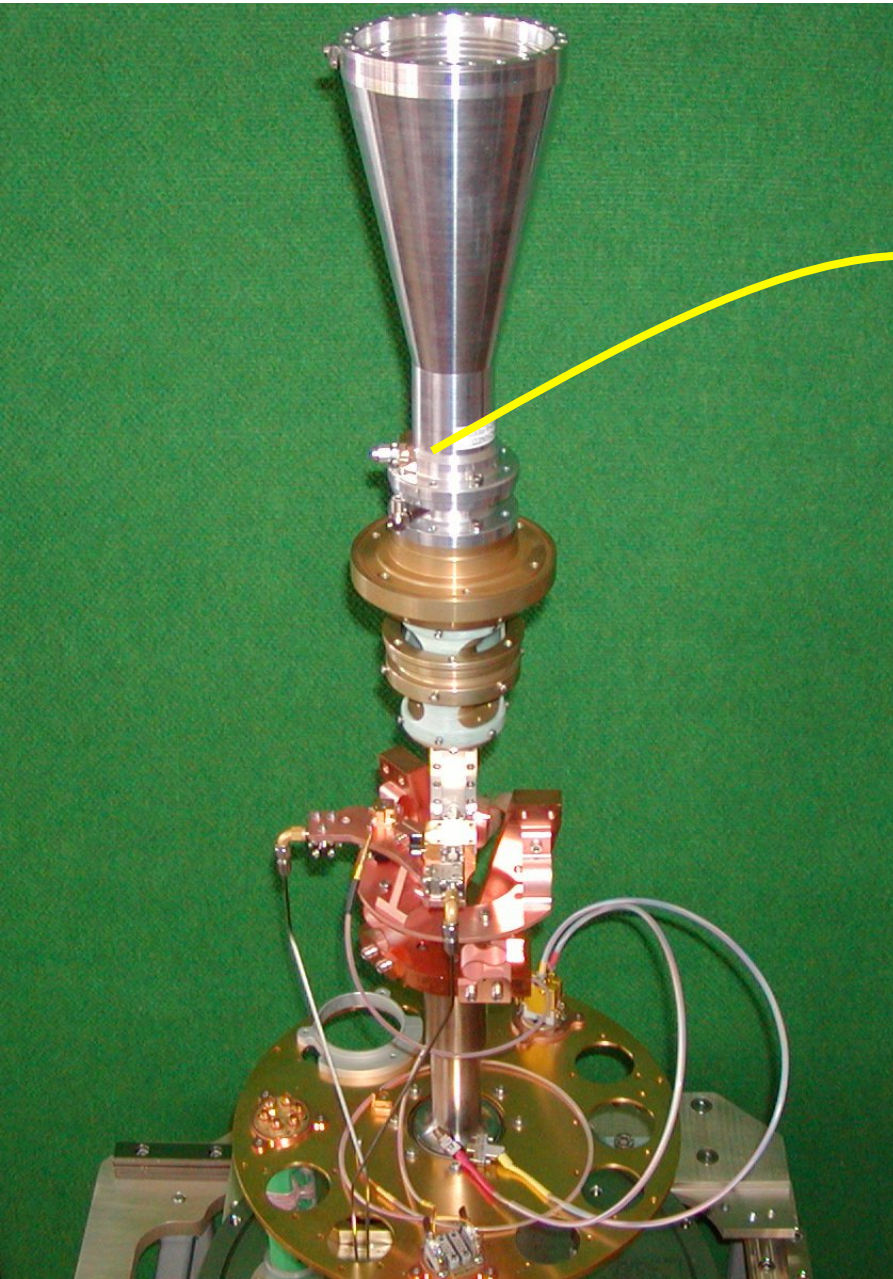
NAR – noise- adding radiometer

Jargon:

“noise tube”
= “noise diode”
= “noise source”
= “cal”



ANAL PATH - THE RECEIVER SYSTEM - Sinclair, et al



MONITOR & CONTROL

POWER SUPPLY VOLTAGE

R.F. OUTPUT

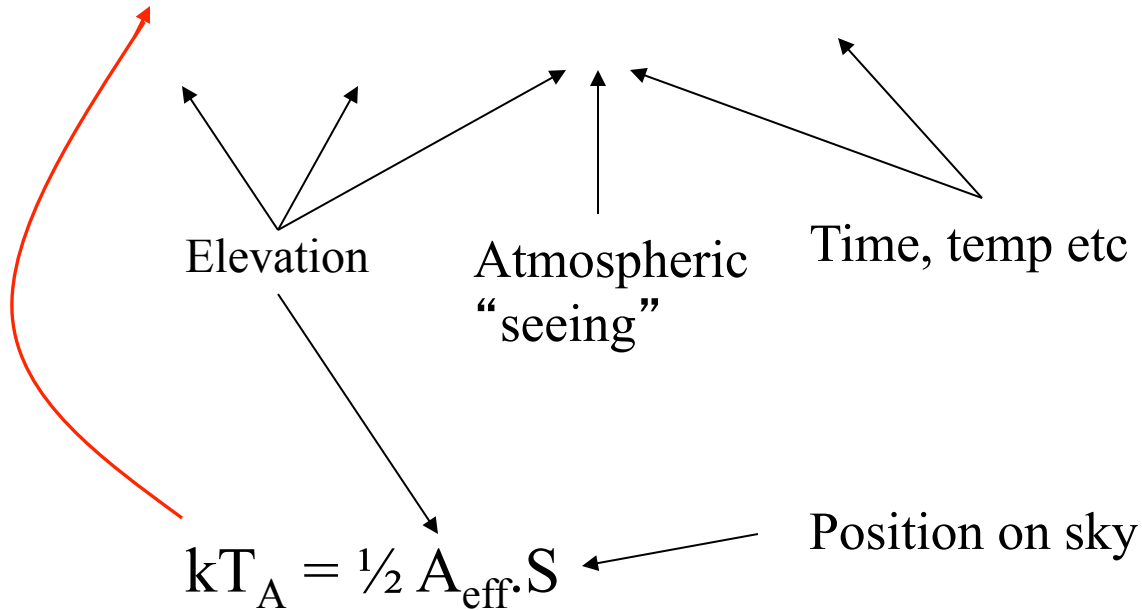
240V A.C.

R.F. OUTPUT

HELIUM SUPPLY

The noise equation

$$T_{\text{sys}} = T_A + T_{\text{spill}} + T_{\text{sky}} + T_{\text{rx}} + T_{2.7\text{K}}$$



Radiometer Equation

$$SE(T_{\text{sys}}) = \alpha \cdot T_{\text{sys}} / \sqrt{t \cdot \Delta f}$$

where;

t = integration time (seconds)

Δf = detector bandwidth (Hz)

α = factor of order unity (system dependent)

1 sigma (SE) not usually enough \rightarrow 3 or 5 sigma

There's noise and there's noise:

above does not include "flicker" noise

Single-dish calibration

Pointing (at higher frequencies)

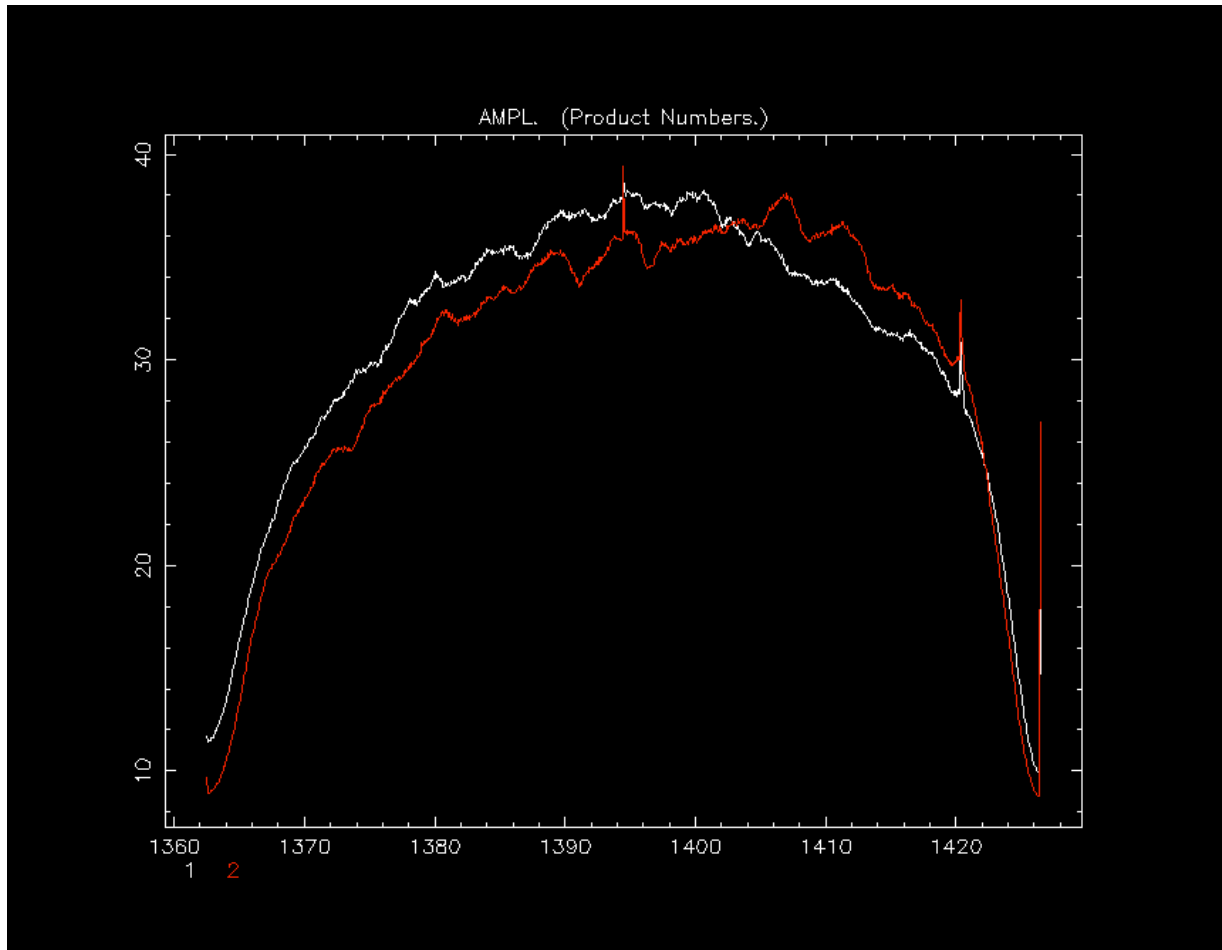
Gain vs Elevation

Tsys vs time

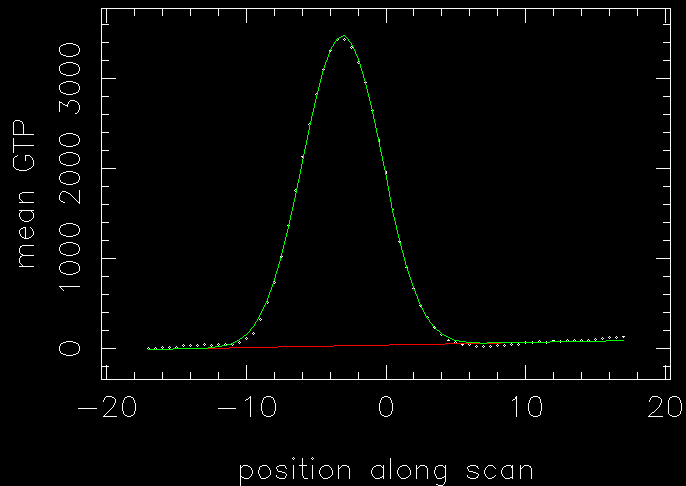
Remove the noise pedestal!

The single-dish millstone

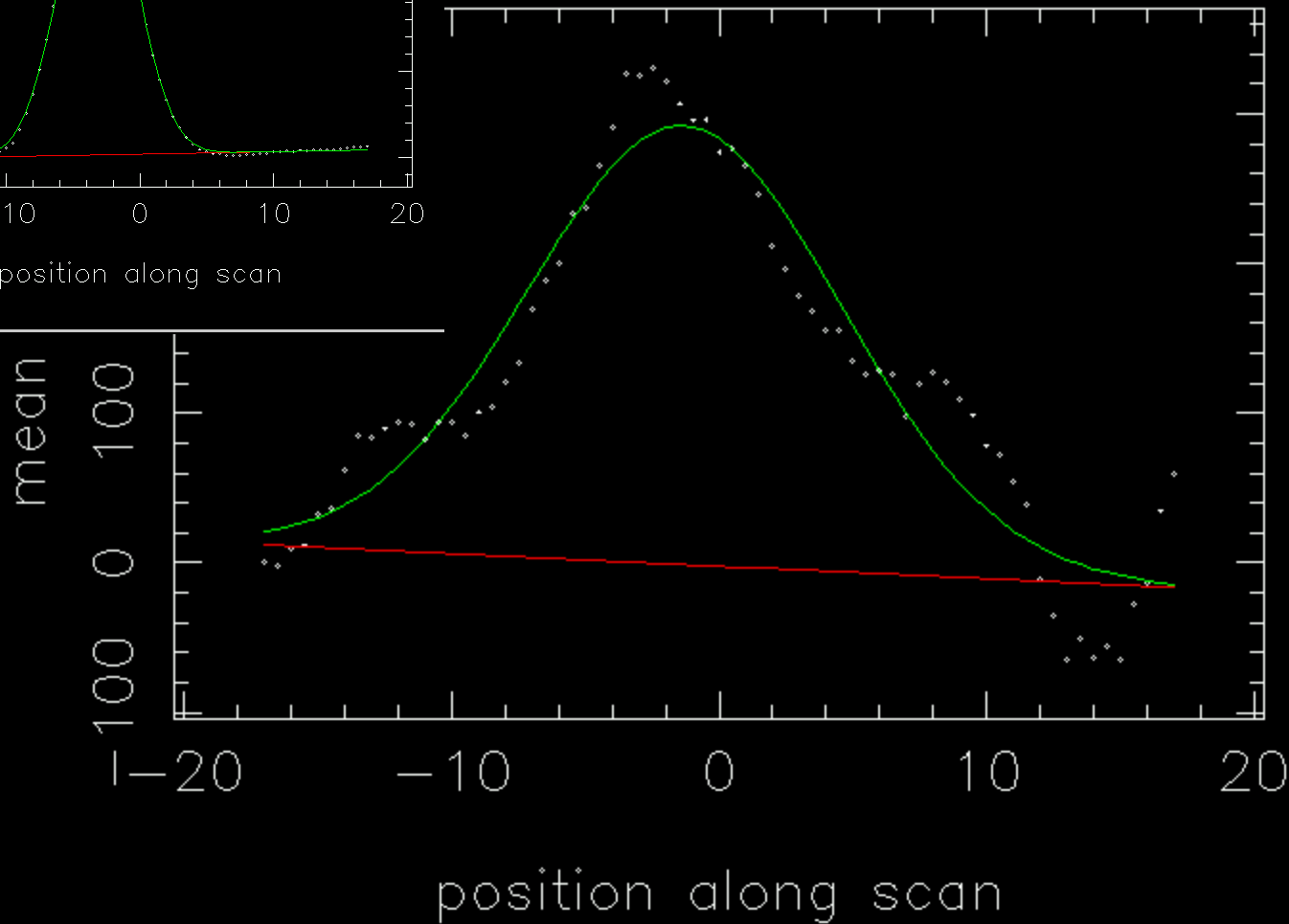
Large and quasi-constant “DC” noise pedestal floor –
Small fluctuations with time/frequency are important!



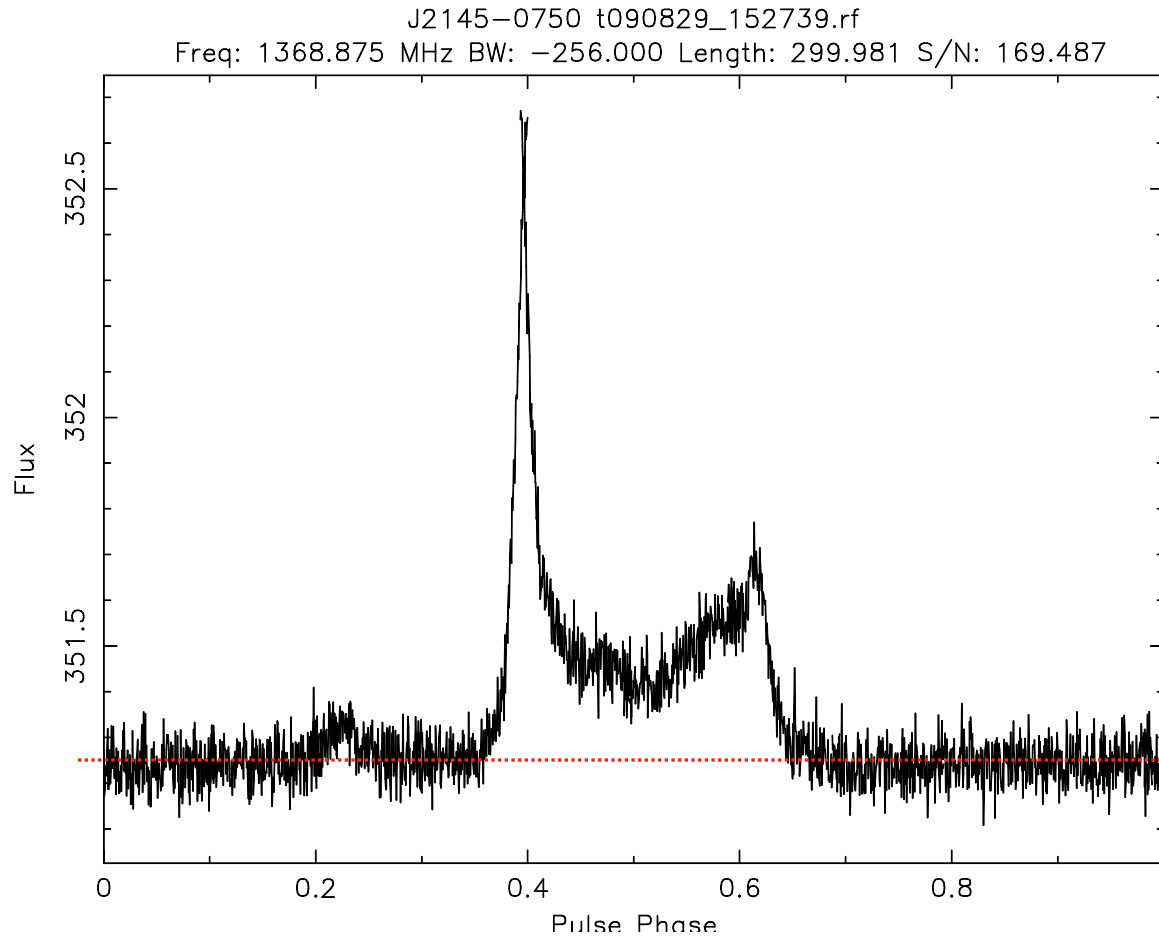
long1 jupiter



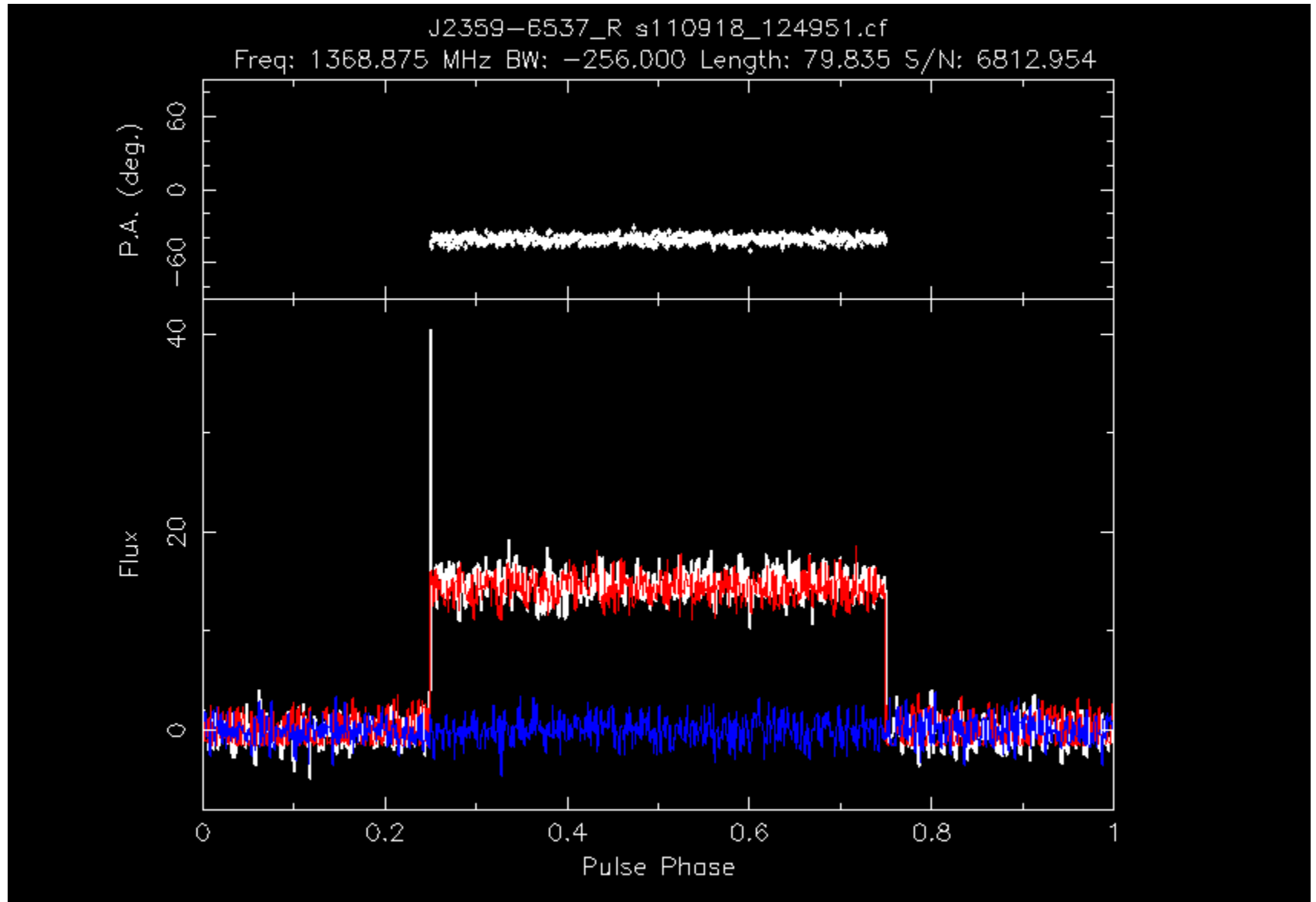
long1 2345-167



Pulsars: average “off pulse” noise;



Single dishes use correlators too

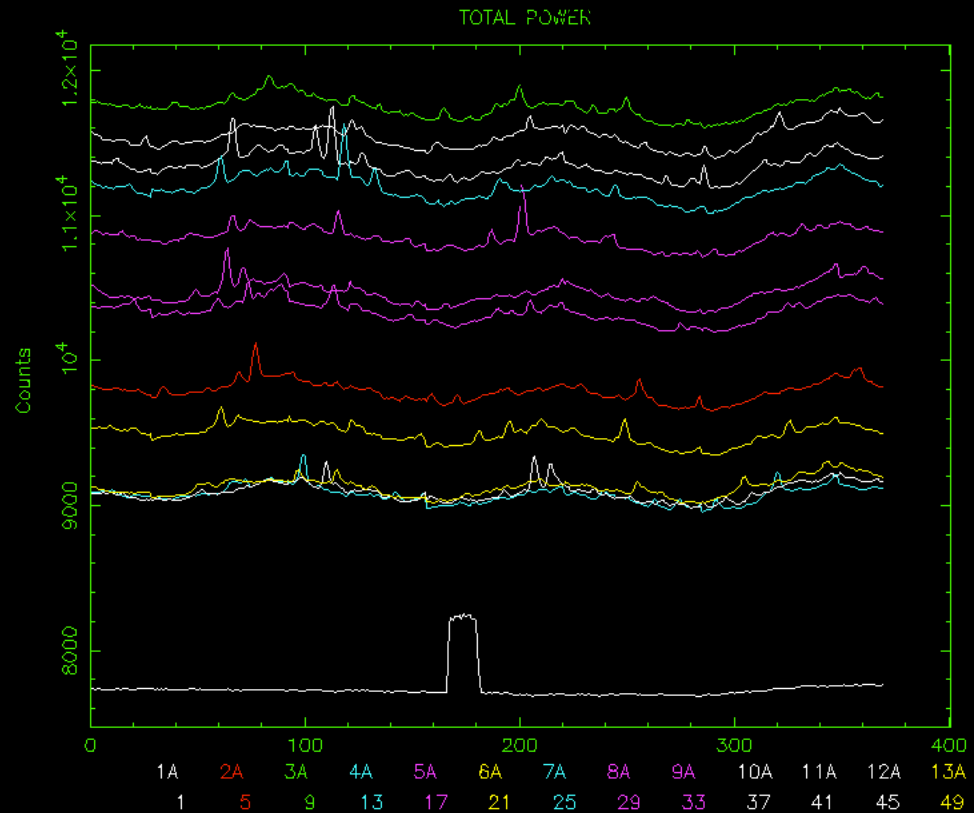
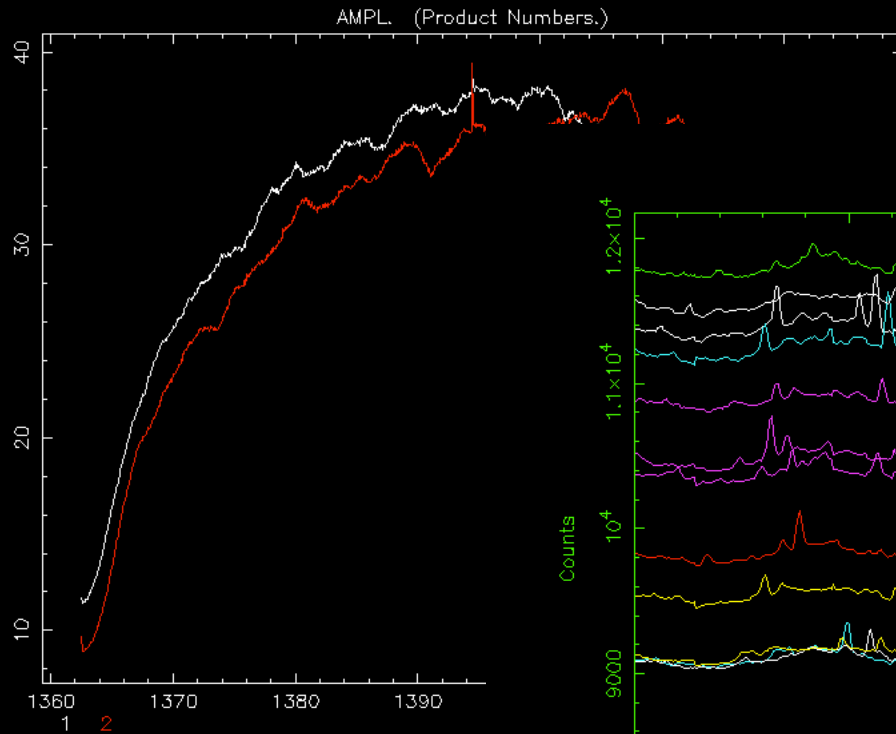


Spectral-line / continuum

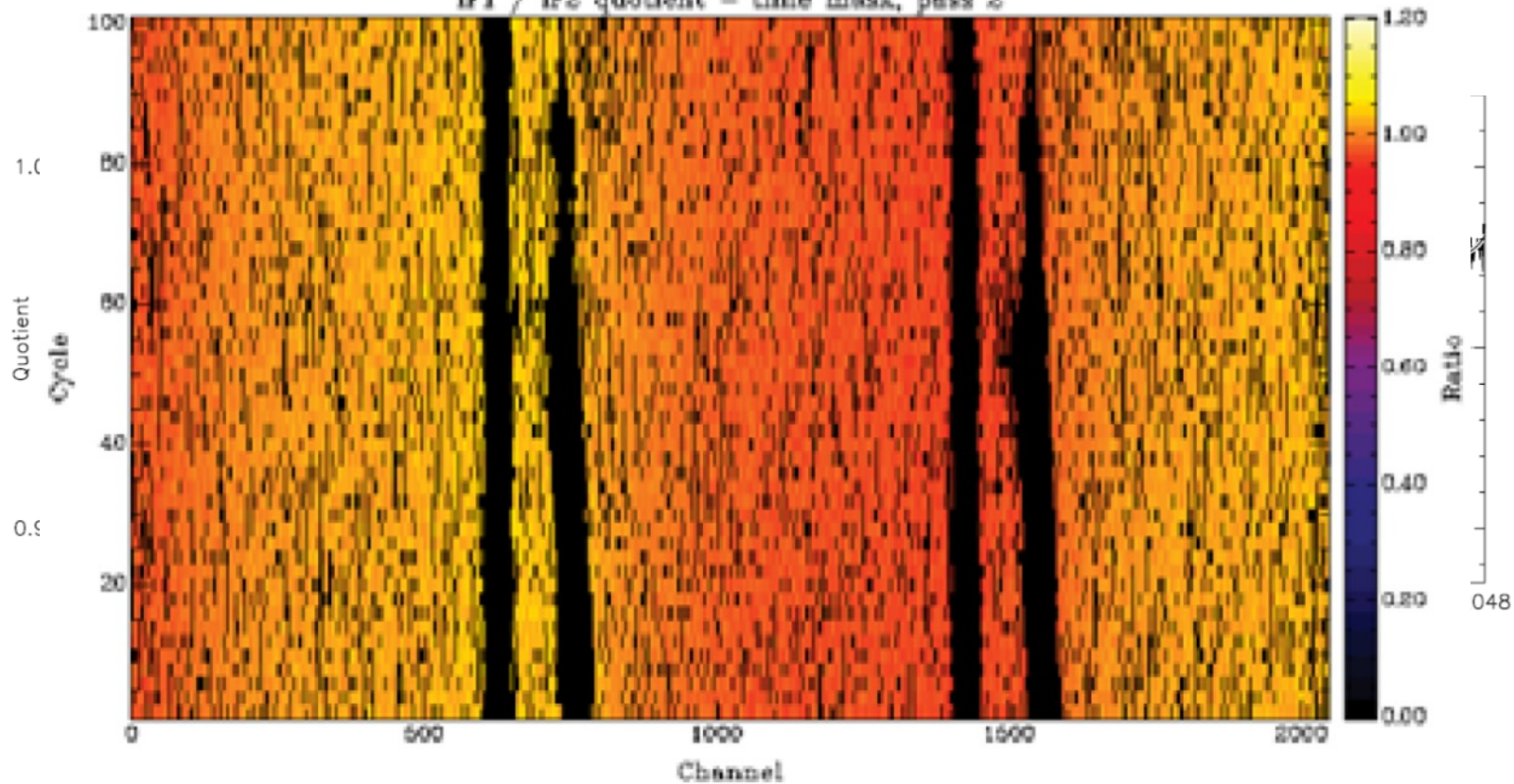
- On source – Off source
 - Switch between on and off-source, subtract/divide
 - “MX” mode on Multibeam receivers
- Frequency shift
 - Switch between two adjacent frequencies, divide
- Scan and average
 - Subtract mean (median) of entire scan

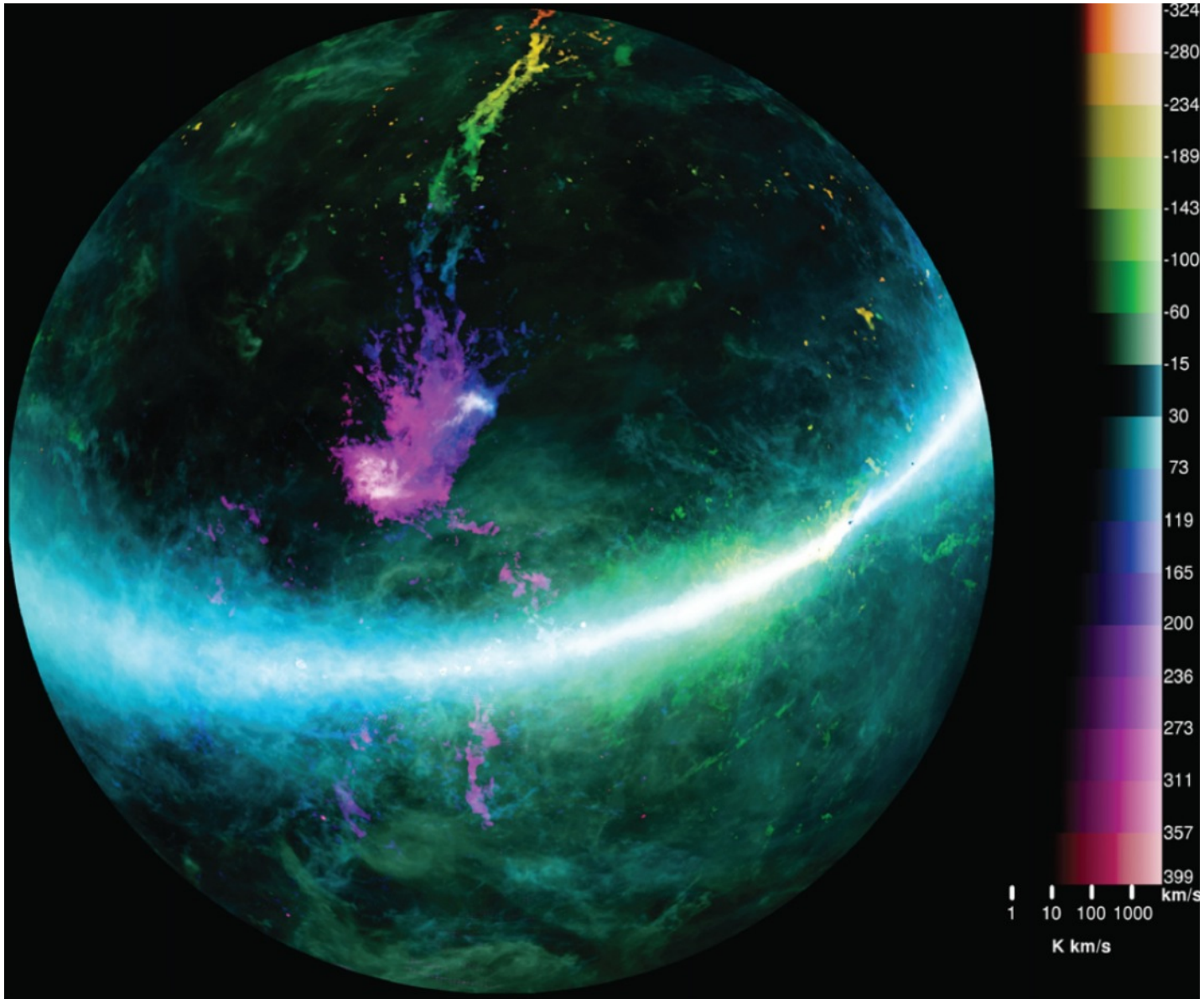
Bandpass calibration

Calibrate bandpass by observing “off



IF1 / IF2 quotient - time mask, pass 2





The End