# The SYN Projection

#### ATNF document series

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#### 1 Introduction

The SYN (synthesis) projection provides an exact coordinate description for any co-planar synthesis array. This includes east-west arrays and VLA snapshots. It includes SIN and NCP as special cases.

SYN has been included in the FITS WCS proposal as a generalization of the SIN projection.

#### 2 Derivation of the SYN projection

From the basic synthesis equation, the phase term in the Fourier exponent is

$$phase = (e - e_0) \cdot B \tag{1}$$

where e and  $e_0$  are the unit vectors pointing towards a point in the field and the field centre, **B** is a baseline vector, and we measure phase in rotations so that we don't need to carry factors of  $2\pi$ . We can write

$$phase = p_u u + p_v v + p_w w ag{2}$$

where (u, v, w) are components of the baseline vector in a coordinate system with the w-axis pointing from the geocentre towards the source and the u-axis lying in the J2000.0 equatorial plane, and

$$p_{u} = -\cos\theta\sin\phi$$

$$p_{v} = -\cos\theta\cos\phi$$

$$p_{w} = \sin\theta - 1$$
(3)

are the coordinates of  $(e - e_0)$ , where  $(\phi, \theta)$  are the longitude and latitude of e in the (left-handed) native coordinate system of the projection with the pole towards  $e_0$ . Now, for a planar array we may write

$$n_{\mathbf{u}}u + n_{\mathbf{v}}v + n_{\mathbf{w}}w = 0 \tag{4}$$

where  $(n_u, n_v, n_w)$  are the direction cosines of the normal to the plane. Then

$$w = -\frac{n_u u + n_v v}{n_w} \tag{5}$$

Combining (2) and (5) we have

phase = 
$$[p_u - \frac{n_u}{n_w} p_w] u + [p_v - \frac{n_v}{n_w} p_w] v$$
 (6)

From equations (3) and (6) the equations for the "SYN" projection for a planar synthesis array are thus

$$x = -[\cos\theta\sin\phi + p_1(\sin\theta - 1)]$$

$$y = -[\cos\theta\cos\phi + p_2(\sin\theta - 1)]$$
(7)

where

$$p_1 = n_u/n_w$$

$$p_2 = n_v/n_w$$
(8)

## 3 SYN projection equations in equatorial coordinates

If  $(\alpha, \delta)$  and  $(\alpha_0, \delta_0)$  are the J2000.0 right ascension and declination of e and e<sub>0</sub> then

$$\cos \theta \sin \phi = \cos \delta \sin(\alpha - \alpha_0)$$

$$\cos \theta \cos \phi = -\sin \delta \cos \delta_0 + \cos \delta \sin \delta_0 \cos(\alpha - \alpha_0)$$

$$\sin \theta = \sin \delta \sin \delta_0 + \cos \delta \cos \delta_0 \cos(\alpha - \alpha_0)$$
(9)

These may be substituted into equations (7) to obtain the SYN projection equations in J2000.0 equatorial coordinates.

### 4 Special cases of the SYN projection: SIN and NCP

Note in equations (7) that since theta is approximately 90° the terms involving  $p_1$  and  $p_2$  are small; neglecting them, as is usually done, gives us the equations for the "SIN" projection:

$$x = -\cos\theta\sin\phi \tag{10}$$

$$y = -\cos\theta\cos\phi$$

From equations (7), for an array which lies in the J2000.0 equatorial plane, we have

$$n_{u} = 0$$

$$n_{v} = \cos \delta_{0}$$

$$n_{w} = \sin \delta_{0}$$
(11)

where  $\delta_0$  is the declination of the field centre, whence

$$p_1 = 0$$

$$p_2 = \cot \delta_0$$
(12)

 $\mathbf{and}$ 

$$x = -[\cos\theta\sin\phi]$$

$$y = -[\cos\theta\cos\phi + \cot\delta_0(\sin\theta - 1)]$$
(13)

These are the equations for the "NCP" projection. To first order the difference between equations (10b) and (13b) is

$$\frac{r^2}{2}\cot\delta_0\tag{14}$$

where r is the distance from the field centre in radians. This amounts to nearly 1' for a position 1° from the field centre at  $\delta_0 = 30^{\circ}$ .

### 5 Correction for precession

The plane of an east-west array coincides with the apparent equatorial plane at the date of the observation and this is tilted slightly with respect to the J2000.0 equatorial plane. If  $(\alpha_p, \delta_p)$  are the J2000.0 right ascension and declination of the apparent pole then

$$n_{u} = -\cos \delta_{p} \sin(\alpha_{p} - \alpha_{0})$$

$$n_{v} = \sin \delta_{p} \cos \delta_{0} - \cos \delta_{p} \sin \delta_{0} \cos(\alpha_{p} - \alpha_{0})$$

$$n_{w} = \sin \delta_{p} \sin \delta_{0} + \cos \delta_{p} \cos \delta_{0} \cos(\alpha_{p} - \alpha_{0})$$

$$(15)$$

4

These may be substituted directly into equations (7) and (8). Precession from 1990 to 2000 amounts to about 3'. For  $\alpha_p = \alpha_0$  and  $\delta_0 = 30^\circ$  we get

$$p_1 = 0$$

$$p_2 = 1.72857$$

Equations 12 with no precession correction give

$$p_1 = 0$$
 $p_2 = 1.73205$ 

For a position 1° from the field centre at this declination the difference between these amounts to about 0".1.

#### 6 Field shifts

A phase shift may be applied to the visibility data at the time a map is synthesized in order to translate the field centre. If the phase shift applied to the visibilities is

$$phase shift = q_u u + q_v v + q_w w$$
 (16)

where  $(q_u, q_v, q_w)$  is constant then equation (2) becomes

$$phase = (p_u - q_u)u + (p_v - q_v)v + (p_w - q_w)w$$
(17)

whence equation (6) becomes

phase = 
$$[(p_u - q_u) - p_1(p_w - q_w)]u + [(p_v - q_v) - p_2(p_w - q_w)]v$$
 (18)

Equations (7) become

$$x = -[\cos \theta \sin \phi + p_1(\sin \theta - 1)] - [q_u - p_1 q_w]$$

$$y = -[\cos \theta \cos \phi + p_2(\sin \theta - 1)] - [q_v - p_2 q_w]$$
(19)

From which we see that the field centre is shifted by

6 FIELD SHIFTS

$$\Delta x = q_u - p_1 q_w 
\Delta y = q_v - p_2 q_w$$
(20)

The shift is applied to the coordinate reference pixel. For the SIN projection  $(p_1, p_2) = (0, 0)$  and the shift is just

$$\Delta x = q_u 
\Delta y = q_v$$
(21)

For the NCP projection the shift is

$$\Delta x = q_u 
\Delta y = q_v - q_w \cot \delta_0$$
(22)

In the general case the correction for precession, although small, applies systematically to the whole field. For a shift of 1° at  $\alpha_0 = \alpha_p$ , and  $\delta_0 = 30^\circ$  the whole map is shifted by about 0".1 in declination.